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SELECTED DESIGN PARAMETERS FOR RECLINING SEATS BASED ON ENGINEERING ANTHROPOMETRY

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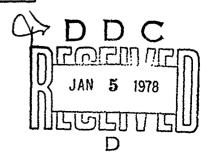
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FOR THE COMMANDER

CHARLES BATES, JR.

Chief

Human Engineering Division

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SECURITY CLASSIFICATION OF THIS PAGE (When Date Entered) READ INSTRUCTIONS BEFORE COMPLETING FORM REPORT DOCUMENTATION PAGE 2. GOVT ACCESSION NO. 3 PECIPIENT'S CATALOG HUMBER TR-77-44 TITLE (and Subtitle) REPORT & PERIOD COVERED SELECTED DESIGN PARAMETERS FOR RECLINING SEATS Final Repert BASED ON ENGINEERING ANTHROPOMETRY. M. M. Ayoub (Texas Tech U) S. Deivanayagam (Texas Tech U) C5013 / mile Kenneth W. Kennedy (AMRL) Dept. of Industrial Engineering Texas Tech University Lubbock, TX 79409 CONTROLLING OFFICE NAME AND ADDRESS 12. REPORT DATE Aerospace Medical Research Laboratory, Aerospace Sentember 1977 Medical Division, Air Force Systems Command, Wright-Patterson Air Force Base, Ohio 45433 162 14. MONITORING AGENCY NAME & ADDRESS(if different from Controlling Office) Unclassified DECLASSIFICATION DOWNGRADING SCHEDULE 16. DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution unlimited. 17 DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report) 18. SUPPLEMENTARY NOTES 19 KEY WORDS (Continue on reverse side if necessary and identify by block number) Aircraft Cockpit Geometry Anthropometry Engineering Anthropometry High Acceleration Cockpits Body Support Systems Aircraft Seats 20 ABSTRACT (Continue on reverse side if necessary and identify by block number) This report discusses selected engineering anthropometric design criteria for reclining cockpit seats. The reclining back-rest positions selected were 13°, 27°, 51° and 65° from the vertical line through the seat reference point (SRP). To seat pan angles of 10 and 20 were utilized. Three seating components were considered in this report, these are: the head rest, arm rest, and foot rest. The specific engineering

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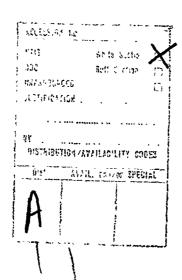
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anthropometric design parameters addressed were: (a) The head rest hinge point location, (b) arm rest location and orientation in space as the seat reclines, (c) location of foot rests and (d) the synchronization of arm rest movement with back rest inclination.



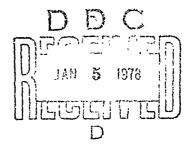


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INTRODUCTION

Background

The recent technological advancements in the design of fighter aircraft have resulted in planes which can withstand high G loadings. Therefore, the "High Performance Fighter" has the capability for improved maneuverability resulting in increased demands on the pilot. These planes can sustain the high G loading (up to 15 G) for a considerable period of time. Such capability gives a decisive advantage over the enemy in tactical combat missions, both offensively and defensively (Kulwicki & Sinnett [1]). However, these high G environments can exceed the physiological limits of the pilot and therefore, render him less effective as a component of the weapon system. In essence, even though the technology has been developed to produce an aircraft with superior performance capability, lacking the pilot ability to cope with the super G, results in a system performance short of optimum.

The simple fact is that a fighter pilot in the standard aircraft seat configuration has limited tolerance to withstand high normal acceleration forces (G_Z) , (Physiology of Flight [2], Bioastronautics Data Book [3]). This is because the "downward g" acceleration pools the blood supply in the lower part of the body and severely curtails the supply to the head. The pilot then experiences "gray out" and "black out" depending on the level and duration of the G environment. This problem can be overcome to a certain extent by wearing an anti-G suit. Special breathing procedures

(M-1 technique, Valsalva method) can also be employed to alleviate the effect of G forces to a certain extent. But these procedures are not effective at G loads beyond about 8 G. Hence recently, serious attention has been directed toward the concept of changing the posture of the pilot from upright towards supine so that the "hydrostatic head" required to supply blood to the pilot's head is reduced. Figure 1 shows this effect pictorially.

This concept is not new. Gell, et. al., [4] report a centrifuge study in which the back rest was varied (up to 85°) in the rear cockpit of a Navy F-7 fighter. The G tolerance of the subject increased beyond 45°, and at 85°, was recorded as 15 G for a period of five seconds.

Crossley, <u>et. al.</u>, [5] report an increase in gray out threshold as back angle was changed from 15° to 70° to a maximum of 8 G.

Von Beck [6] lists the following as the three "desirable" design characteristics for a tilt seat:

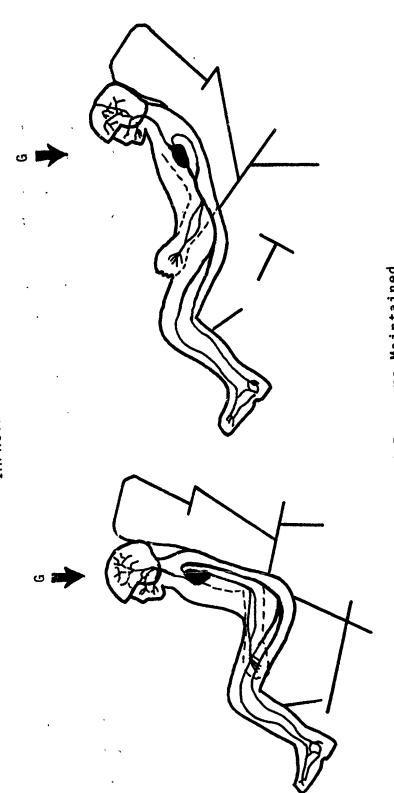
- 1. Maintenance of forward visibility.
- 2. Control and instrument location.
- 3. Emergency escape system.

He also notes that the pilot should be able to land and take off while reclined.

Replogle, et. al., [7] conducted a centrifuge study using a simulated air combat task to measure the performance of the pilots. Results showed that at 9 G with 65° back angle, the performance was equivalent to that at 7 G with 13° back angle. They also report a lowered heart rate, improved "G on G" performance and subject acceptance of larger back angles.

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RECLINED POSITION IMPROVES HIGH G BLOOD SUPPLY



Eye Level Blood Pressure Maintained Reduced Blood Pooling Lower Heart Rate

Figure 1

[from Kulwicki, P. V. and Sinnett, J. M., "The High G Approach" MDC A2109, McDonnell Douglas Aircraft Co., 1973]

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Similar beneficial effects were also reported with a reclined seat back under transverse (G_y) acceleration by a number of authors. Taking advantage of these benefits of reclining the pilot on his back to improve the G tolerance, a new approach in cockpit design is being considered. Thus, the "High Acceleration Cockpit (HAC)" concept requires that the pilot assume a 65° or larger back rest position under high G environment. Figure 2 shows the improvement possibility in human tolerance to G forces with a 65° back rest angle. The high G tolerance thus achieved can be put to best use by the pilot to make better utilization of the aircraft capability and gain a specific advantage over his adversary in a tactical combat situation.

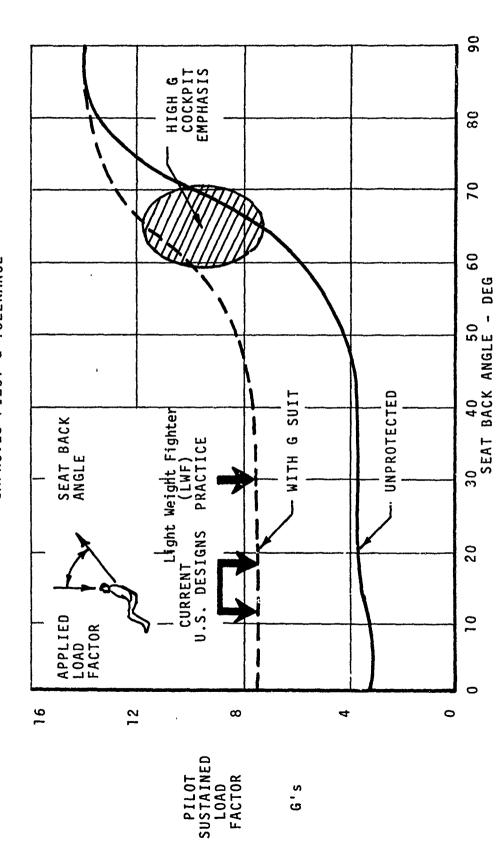
While such a tactical superiority can be achieved on G tolerance basis, certain other problems are encountered by a supine pilot. The reduction in forward visibility is a very critical one. The pilot can lose a certain amount of over the nose vision and panel vision as compared to upright seat position. To minimize this effect, the HAC concept calls for raising the seat and rotating the head forward (by rotating the head rest by about 40°). This results in a minimum over the nose vision of -10°. Secondly, the supine position will call for the utilization of new types of controllers. Finally, body movement under G environment itself may produce labyrinthine symptoms [9].

Purpose and Scope of the Study

This study was undertaken to generate engineering/anthropometric data base for the design of head rests, arm rests, and foot rests for high acceleration cockpit seats of the articulating type to insure optimum comfort for

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RECLINED POSITION IMPROVES PILOT G TOLERANCE



[from Kulwicki, V.P. and Sinnett, J. M., "The High G Approach" MDC A2109, McDonnell Douglas Aircraft Co., 1973] Figure 2

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the pilot under dynamic conditions without sacrificing any comtat performance capability. The specific requirements are to provide proper support of the body and limbs under upright, supine and transient conditions. At the same time:

- (1) Permit head movement to maintain all-around visibility.
- (2) Permit hand and foot mobility to operate essential controls for high G maneuvering of the aircraft.

It is also required that these rests should have adjustability for the comfort of the individual pilot, taking into account pilot population size.

APPROACH

In order to objectively achieve a feasible design for the head rest, arm rest, and foot rest for the high G cockpit seat configurations several design criteria have been selected for each of the components to be designed.

1. Design Criteria

- a. <u>Head rest</u>: Based on the changes in seat configurations from the standard 13° back rest to the new high G concept of 65° back rest, the head rest should be designed to:
 - ·provide maximum comfort to the pilot
 - cause minimum interference with personal equipment used by the pilot
 - provide optimum visibility
 - provide freedom of head movement commensurate with visual requirements (or have a mechanized head rest)
 - be compatible with ejection seat requirements
 - provide adjustability to accommodate the pilot population

- b. Arm rest: Since the new high G seat configuration makes it impossible to use "conventional" flight controllers, new controller designs have been proposed [8, 10]. These controllers will likely be mounted on arm rests and operated with the hand and fingers. Therefore, arm rests should be designed to:
 - ·provide the needed support for the entire upper extremity
 - ·cause no interference with the operation of essential controls mounted on these arm rests and immediately adjacent surfaces
 - •provide upper extremity configurations conducive to maximum biomechanical advantage
 - ·meet ejection seat requirements
 - ·provide individual adjustability
 - ·be synchronized with seat configuration changes
- c. <u>Foot rest</u>: Under high G environment, the pilot in the proposed seat configuration must be provided with heel support. It will serve to keep the pilot's feet on the rudder controls, especially under high G levels. The foot rest should be designed to:
 - provide support to maintain the position of the feet on the rudder controls throughout their ranges of movement
 provide adjustability
 - ·meet the ejection seat requirements, if any
 - •maintain reasonable foot-tibia relationship--to minimize
 any detrimental effect on performance

2. Design Parameters

For each of the head rest, arm rest, and foot rest, there are a few basic individual design parameters that must be considered. The following section discusses these parameters for each.

a. Head rest:

- (1) Shape: The head rest must be shaped to provide support to the head (also neck support, if needed). Proper support will have to be provided to the head with its protective gear at the upright and the full range of reclined positions.
- (2) <u>Size</u>: Head rest size will be kept as small as possible to minimize interference with lateral and rear visibility. At the same time, it should provide the necessary support at the required areas. Further, the size and shape, as well as freedom of movement requirements, would also determine whether support over the neck area is advantageous.
- (3) <u>Hinge Point</u>: Hinge point is the point about which the head rest must articulate relative to the back rest. This point has to be at the proper position with respect to the torso to provide comfort and safety upon ejection and at the same time not cause interference with personal protective clothing when the seat is in the fully reclined configuration.
- (4) Range of Movement: Range of movement of head determines the total visibility envelope. Therefore, the head rest should permit movement of the head to meet the minimum visibility requirements, while maintaining the proper support.

(5) Adjustability: The head rest should have enough adjustability to accommodate the range of body sizes found in the USAF pilot population.

b. Arm rest:

- (1) <u>Shape</u>: The proper shape and contour to support forearm and controls and to permit easy operation of these controls has to be considered.
- (2) <u>Size</u>: The arm rests should provide enough support area for the upper extremity and not interfere with the operation of controls or ejection procedure.

The arm rest should be as small as possible, but at the same time, it must provide adequate support and stability for the arms and space for control instrumentation.

- (3) General Location and Orientation: The elevation, bearing, and fore-aft positioning of the arm rests should permit optimum control manipulation and comfort. The ejection procedure requirement also has a definite effect on the location of arm rests.
- (4) Adjustability: Enough adjustability must be provided for the range of pilot population.
- (5) Synchronization: The arm rest should be synchronized with back rest movement (i.e., from 13° to 65° configurations) to provide the same control location with respect to upper arm configurations at these extreme positions as well as during the transitional movements.

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c. Foot rest:

- (1) Shape: The foot rest should be shaped to provide enough support at the heel without hindering the foot operation at the rudder pedals under normal or under high G environments.
- (2) <u>Size</u>: The foot rest must be large enough to cover the range of heel positions possible, whether the pilot is in the upright or reclining position.
- (3) Orientation with Respect to Foot Control: The spatial orientation of the rest should not interfere with the foot control operation at both upright and supine positions. The foottibia angle changes from upright to reclined position.
- (4) Adjustability: There should be enough built-in adjustability to cover the range of pilot population.

The following section will describe the equipment used to generate the required data as well as the equipment used to reduce and digitize these data.

EQUIPMENT

The major pieces of equipment used in this study were: The AMRL photogrammetric system, the digitizing equipment, and the experimental seating/controller positioning device. Of these, the photogrammetric system and the digitizing equipment have been used earlier. A complete description of these may be found in Ayoub, et. al., [14].

Photogrammetric System

The photogrammetric facility used in this study was designed and built at the Aerospace Medical Research Laboratory of U.S. Air Force. A schematic layout of the system is shown in Figure 3. In essence it consists of two pairs of front surface, minimum distortion mirrors and a 70 millimeter fast sequence camera with strobe units. The components of the system are so laid out as to obtain two orthogonal view images of a task area on a single frame of picture. For additional detailed information, see reference [14].

<u>Digitizer Unit</u>

A Viable Systems x-y digitizer unit was employed to extract coordinates from the film projections. It consists of a 70 mm projector, a rear projection screen with a mirror, a x-y digitizer with a movable cursor and a paper tape punching unit. The system was assembled using commercially available components. Figure 4 shows the x-y digitizer unit.

Targets

The skin surface points were identified by suitable surface type target or extension type targets. Surface type targets were made up of adhesive . I tape in black and white and were directly attached to the skin.

At locations where surface type target may not be seen in both views of the picture extension type targets were used. An extension type target consists of thin white plastic tube 1/4" diameter and either 3" or 1.5" long. Figure 5 shows an extension type target 3" long. The ratio of distances AB to BC is 1:2. Thus, if the locations of A and B can be

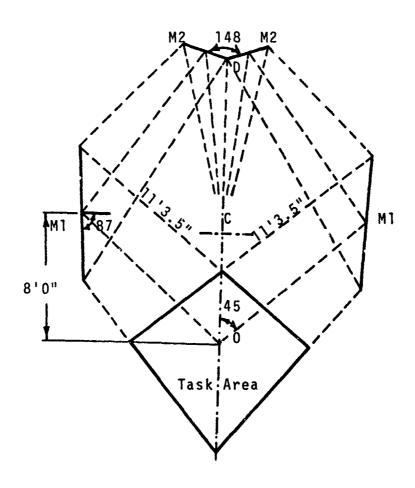


Figure 3 Schematic Layout of Photogrammetric System

M1 - 7'3.5" sq. Mirror
M2 - 2'6" sq. Mirror
C - Camera. 0 - Center of Task Area
CD - 9'7.25". OC - 6'7.25"

(Modified from the original drawing by K. W. Kennedy, AMRL, Wright-Patterson AFB, Dayton, OH)

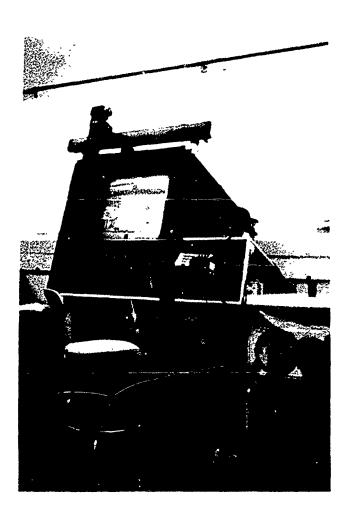


FIGURE 4 THE VIABLE SYSTEMS X-Y DIGITIZER

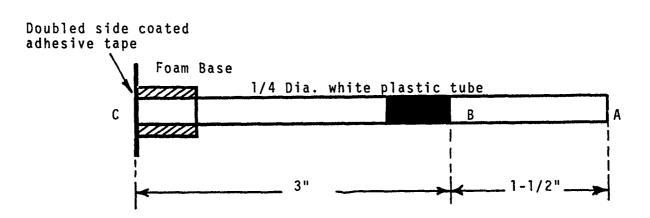


Figure 5 Extension Target (Long 1:2)

determined from the orthogonal views, then the location of skin surface point C can be computed. The point C was always attached to the skin surface point using suitable foam rubber base and adhesive tape.

Seating/Controller Positioning Device

The seating/controller positioning device was specially designed and fabricated at AMRL facilities for this study. It was designed to provide flexibility to change back rest and seat pan configurations, and hand controller and foot controller locations. Figure 6 shows the general arrangement of the seating device along with hand and foot controllers.

Seat Configuration Capability

The seat can be adjusted to provide the following configurations as a function of seat pan, back rest, and head rest angles:

- Back rest angle 0° to 70° measured backwards from vertical (backwards).
- 2. Seat pan angle 0° to 30° measured upward from horizontal.
- 3. Head rest angle 0° (flush with back rest) or 30° (forward of back rest measured from plane of back rest).

Suitably mounted hydraulic jacks provided the basic mechanisms for back rest angle and seat pan angle adjustments. The back rest was made in two segments with provision to adjust the length of back rest from 17" to 25". (See Figures 7 and 8.) This provides adjustability of both the back rest length and the position of the hinge point of the head rest.

Hand Control Location Adjustments

A vertical cylinder 1.5" in diameter and 4" long represented a hand controller. The controller can be located at different points in space

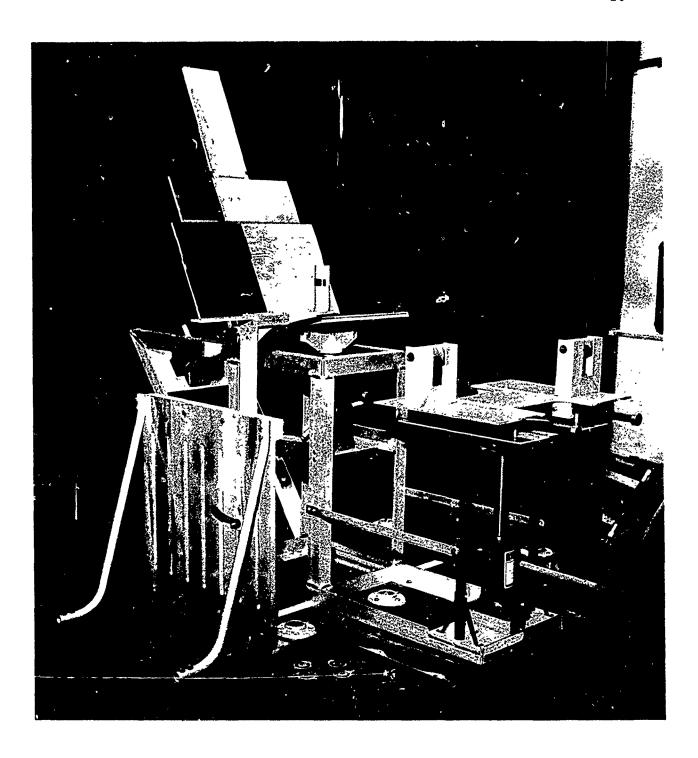


Figure 6 General Arrangement of the Seating Device

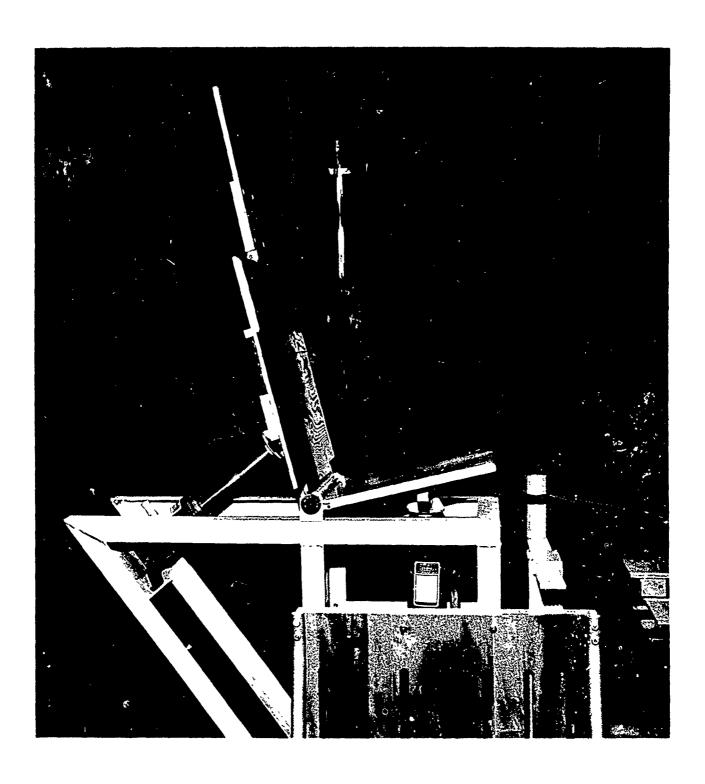


Figure 7 Using Hydraulic Jacks Back Rest and Seat Pan Adjustment Mechanisms

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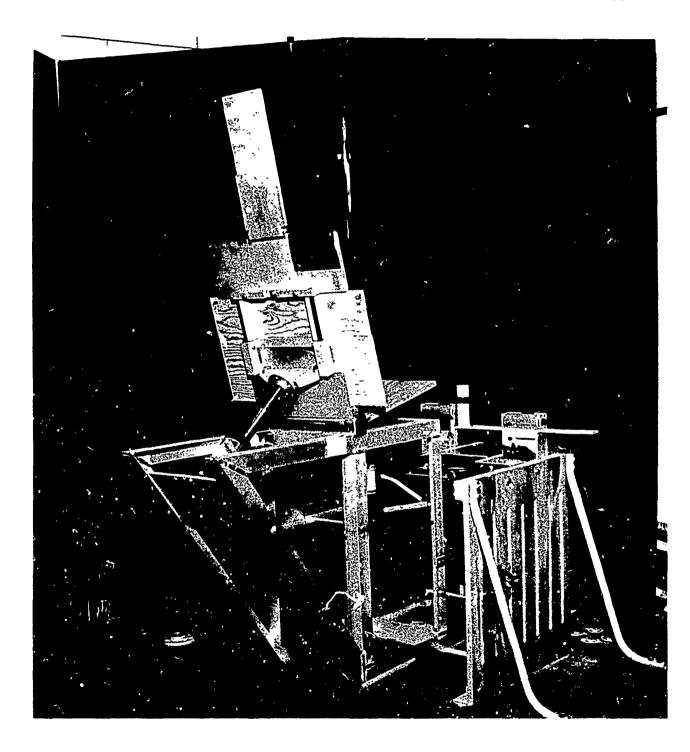


Figure 8 Back View Showing Back Rest and Head Rest and Provisions for Back Rest Length Adjustment

with respect to the Seat Reference Point (SRP) within the following extreme positions:

Fore - aft: +24" to -4"

Up - down: +15" to +3"

Left - right: -3" to -18" (negative coordinate indicates the adjustment

was possible on right side only)

The hand controller was supported by means of suitable hardware to provide the needed adjustments. The hand controller was provided on the right hand side of the chair. (See Figure 9.)

Foot Control Adjustment

Two horizontal cylinders 2" in diameter x 6" long represented rudder pedals to be operated by feet. They were mounted on a sliding platform directly in front of the seat. The axes of the pedals were at a height of 5" from the top surface of the sliding platform. A horizontal separation of 18" center to center was maintained between right and left pedals. The pedals can be positioned and locked individually on the sliding platform at 1" intervals over a range of 10" along the fore-ait direction. The sliding platform itself has provision for movement fore and aft, such that a rudder pedal located over the midline of the platform can be positioned from about 30" to 42" forward of SRP. (See Figure 10.)

EXPERIMENTAL DESIGN AND PROCEDURE

Experimental Design

In order to study the effects of upright and semi-reclined body positions on the design requirements of the seat, the five seat configurations shown in Table 1 were selected to be included in the experimental

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Figure 9 Hand Controller With Adjustment Mechanism

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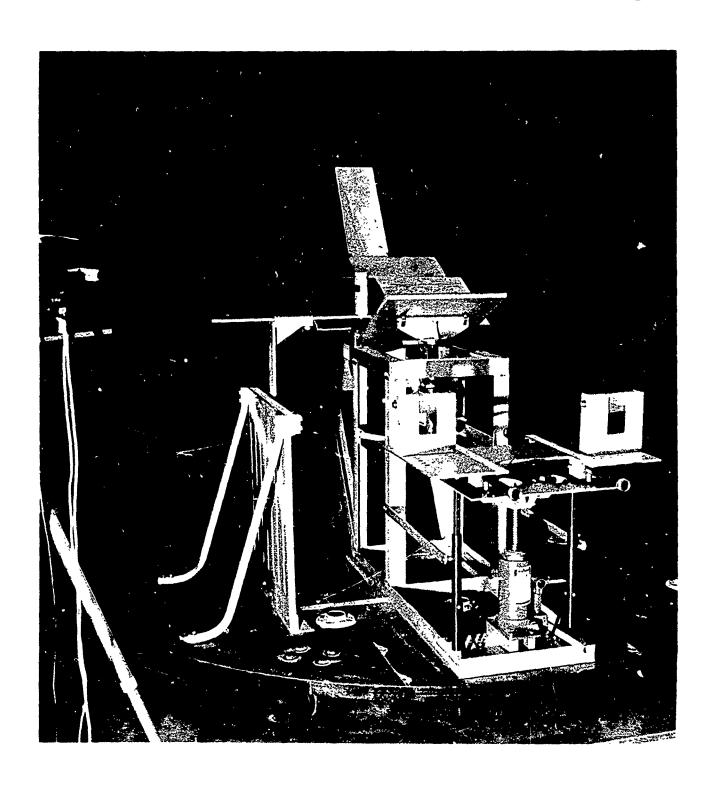


Figure 10 Foot Control Platform and Adjustment Mechanisms

TABLE 1
CHARACTERISTICS OF SEAT CONFIGURATIONS

Seat Configuration	Back Rest Angle	Head Rest Angle*	Seat Pan Angle
I	13°	0°	10°
II	27°	0°	10°
III	51°	30°	10°
IV	65°	30°	10°
V	65°	30°	20°

^{*}Head rest angle measured forward from back rest.

design. Thus the back rest angle chosen for the study are 13°, 27°, 51°, and 65° from the vertical. It was found that at 13° and 27°, the head rest was not essential, but at 51° and 65° back rest angles, the head rest, inclined 30° forward would provide the desired support and comfort to the subject. The fifth seat configuration was different from the fourth in that the seat angle was changed from 10° to 20°. This was done in order to assess the effects of increased seat inclination in providing more area of support to the thighs.

To obtain all the needed data, the experimental design called for three sets of photographs for each seat configuration. These three sets of photographs would relate to head rest, hand rest and foot rest studies, separately. In each of these pictures, the interest was to determine the spatial locations of certain body landmarks. The specific body landmarks considered are listed in Table 2.

Subjects

A total of 24 subjects participated in the study. Of these, three subjects did not participate in the head and upper torso part of the study (see page 35). All the subjects were volunteer male students. They were selected to represent U.S. Air Force pilot population especially with regard to their segment length, i.e. limb and torso. These and other anthropometric characteristics of the subjects are listed in Table 3. Initially, every subject was told about the purpose of the experiment and his responsibilities. Every effort was made to make sure that each subject understood his duties. Table 4 shows a comparison between the subjects' anthropometric characteristics and the corresponding characteristics of the U.S. Air Force flying personnel.

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TABLE 2

SPECIFIC LANDMARKS CONSIDERED IN THIS STUDY

AND IDENTIFIED WITH A TARGET

		Taumah		Study	
	Location	Target Ratio	Head	Hand	Foot
01	Nasion	1:1	*	*	*
02	Menton	surface	*	*	*
03	Supra sternale	1:1	*	*	*
04	Rt. Acromion	1:1	*	*	*
05	Rt. Elbow	1:1		*	
06	Rt. Wrist	1:1		*	
07	Rt. III Meta-Carp.	surface		*	
08	Trochantion, rt.	1:2			*
09	Rt. Knee, top	1:1			*
10	Rt. Knee, pop.notch	1:2			*
11	Rt. Knee, front	surface			*
12	Helmet rear	no Target	*		
13	Upper back	no Target	*		
14	Lower back	no Target	*		

^{*}Indicates the specific landmarks used in the respective part of the study. All landmarks monitored are surface landmarks.

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TABLE 3 ANTHROPOMETRIC CHARACTERISTICS OF THE SUBJECTS

				₹	ANTHROP	Ę					-	-	-	-	-	-	-	_		_		-		_	
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			·																5	12	22	23	Z4 mean	an Dev.	اد ند
	9	8	8	3	8	8	6	8	8	=	=	21	2	+	+-	+	+			2	19	19	23 2	20.9 1.48	8
Age	;	2		23	20	- =	<u> </u>	8	7	72		+	+	+-	+	+;	12 2	2 42 6	1 28	5 167 9	=	9	161.4 160.	0.6 17.0	0.
Weight	156.1	156.1 149.8 15:.3 137.5 134.7 14	15:3	137.5	134.7	2.9	144.4	156.91	168.2	199.2	184.7	182.2 13	137.7 158	9.0 162	5	<u> </u>	, -	1	_		1	1	21 69		54
	72.9	72.9 71.2	71.2	68.3	68.5	7	69.2	70.4	9.69	70.2	70.2	70.0	68.7 68	-	8	27	1	1 5	20 6	29.6		- 5	-	- m	8.
Statute Statute	33.7	33.5	32.7	30.1	29.4	30.1	30.2	32.6	31.1	31.9	32.1	3.1 2.1	30.6	7,	ᅴ	<u></u>	,	3				ļ	7.		233
thoulder-Elbow	15.5	15.3		14.4	13.8	13.7	14.2	15.1	14.8	14.5	14.3	15.0	14.0 14	-	14.2 14.	<u></u>	-	-		2 2	13.6	1, 1	d -	1	- - =
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Acro-Kadiale						١.	9	0	7.0	1.01	8.6	8.6	9.5	9.8	9.8	0.	굮	10.0 10.5	10.5	9.6	릭_	4	-	1	
Radiale-Stylion		10.5	10.8	9.0	<u>,</u>	2,				1	-	-	13.6 13	13.7	13.5 14.	1.5	13.	1.7 14.7	7.	14.2	14.2	13.4	14.2 14	7	22
Elbow-Gr1p	15.1	15.1 14.9	15.1	13.2	₹	13.8	13.0	4.4	-	_	_	, ,	1_	1.	-	3.2	3.3	2.6 3.1	3.	7.6	2.6	2.3	=	300	8
e+v) top-Grin	<u></u>	3.3	3.2	2.7	3.2	3.0	2.9	=	e.			, ,	+;		+	1	39.0 35	136.	9 37.	.2 35.1	37.1	35.6	38.1	36.2	8
Tomeh. Mt.	37.6	36.1	38.6	35.0	35.3	35.6	35.5	37.2	35.2	34.6	36.5	ģ	0.4.0	<u>.</u>		1		+-	1	+-	+	18.7	18.7	18.5	816
1	_		:	;	10,	17 0	17.6	18.8	18.1	18.5	18.7	9 61	1 82	1	89	18.2 20	4	•2	1	-	3		~	31.0	870
Tibiale Ht.	2	20.5 18.5					7		30.0	31.2	31.1	30.1	31.4 3	30.3	32.8 31	~	38.0	30.5 31.	3	7:	<u>: </u>		1	+	
Sttting Eye Ht.	32.6	31.4						1			23.1	23.6	23.9 2	23.1 2	24.9 2	23.9 2	23.1 2	23.1 24.	4 24	.0 23.3	3 23.4	52.6	23.7	2.5	88
Sitting Acromion Ht.	24.6	6 24.0	22.5	22.1	24.8	23.6	2	3					"	3 3	22 3 2	24.4 2	25.8	22.1 23.8	24	.2 22.	2 24.3	22.4	23.8	23.5	676
Sitting Butt-Knee Len.	24.2	2 24.2	24.0	9.22	22.3	3 22.4	23.0	2	23.8	23.8	53.9	°,	,	; †;	1	7	1	21.2 22.	.8 22.0	2	2 2 21.5	21.2	22.7	21.8	.921
Streing To Spinous p. Ht.	Ht 23.1	1 23.0	0 20.9	20.3	22.8	4.12	1.12	122.1	20.9	23.0	21.7	20.7	23.5	N -	•	, ,	; † ;	3	+-	, ,	, ×	"	æ	25.5	.859
Steeing Cervicale Ht.	_	26.0 26.2	24.8	8 23.8	3 25.8	8 24.9	25.0	25.5	24.3	26.7	25.6	24.6	₹	ᆟ	ᇬ	٠,		3 5	+	15		2	0	21.8	.825
Sitting Knee Ht.	+	23.1 21.8 22.3 20.8	8 22.	3 20.8	3 21.0	9.02 0	6 20.9	9 22.8	21.3	22.4	22.0	22.2	21.0	2.0	21.5	7.22	3	1	-	1	4		4	1	
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NOTE: Age is in years; weight is in pounds; other dimensions are in inches.

TABLE 4

STATISTICAL COMPARISON OF THE ANTHROPOMETRIC CHARACTERISTICS

OF THE SUBJECT STUDENT SAMPLE WITH U.S. AIR FORCE

PILOT POPULATION

SAMPLE SIZE = 24

Anthropometric Characteristics	Subject	Sample	U.S.A.F 1967 Survey	
Alletti opolilecti ic character istics	Mean	Std.Dn.	Mean	Std.Dn.
Age - years	20.9	1.48	24.03	2.84
Weight - 1bs.	160.6	17.00	170.00	20.80
Stature - inches*	69.9	1.54	69.88	2.28
Gluteal Furrow Height	31.3	1.40	31.69	1.58
Shoulder - Elbow Length	14.6	0.53	14.09	0.63
Acromion - Radiale Length	13.0	0.53	12.99	0.63
Radiale - Stylion Length	10.1	0.95	10.63	0.55
Elbow - Grip Length	14.2	0.57	13.90	0.59
Stylion - Grip Length	3.0	0.26	Not available	
Trochantion Height	36.2**	1.30	39.97	1.71
Tibiale Height	18.5	0.82	Not available	
Sitting Eye Height	31.0	0.87	31.87	1.19
Sitting Acromial Height	23.4	0.82	23.94	1.10
Buttock - Knee Length	23.5	0.98	23.74	0.98
Sitting T-4 Spinous Process Height	21.8	0.92	Not available	
Sitting Cervicale Height	25.5	0.86	Not avai	lable
Sitting Knee Height	21.8	0.83	21.97	0.94

^{*} All linear dimensions in inches.

^{**} The difference between the study population and the USAF pilots with regard to Trochantion Height appears to be one of technique in measuring.

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Experimental Procedure

The following procedural steps were adopted in recording the needed data on film:

The subject was initially briefed about the experiment and his cooperation was solicited. He removed his clothing except a small brief. The subject wore a standard Air Force helmet and a pair of flight shoes.

'The experimenter measured and recorded all the necessary anthropometric dimensions.

'The specific landmarks were identified and proper targets were affixed on these landmarks.

'A horizontal line at the level of the spinous process of T-4 (4th thoracic vertebra) was drawn on the back of the subject.

'A line joining the right ankle joint and the right knee joint on the lateral surface with the subject standing erect, was also drawn.

The subject was seated on the chair, which was pre-set to one of the five seat configurations described earlier.

After the subject was seated, the back rest/head rest hinge axis was adjusted to the line marking the T-4 spinous process. This adjustment was done for every change in seat configuration.

The experimental procedure was divided into several phases. These are:

.Head and upper torso study,

'Forearm and hand study,

'Foot rest study.

These are presented in the following sections.

Head and Upper Torso

After the subject was seated on the seating device, pictures for head rest and mobility data were taken. For this a head rest angle of 30° (forward) was used in conjunction with back rest angles 65° and 51°. In the cases of 13° and 27° back rest angles, the head rest was in line with the back rest, and subjects did not rest their head on the head rest. The subject was required to be seated centrally on the seat. A thin black tape affixed along the centerline of the seat helped in guiding the subject in positioning himself centrally. The subject rested his feet on the foot control platform and rested his arms on his thighs in comfortable positions. While in this basic configuration, six photographs were taken in sequence for the following head/neck postures:

- 1. Subject's head was in a natural erect posture while looking straight ahead.
 - 2. Subject's head was flexed along midsagittal plane.
 - 3. Subject's head was hyperextended along the midsagittal plane.
- 4. Subject's head was rotated to the right and looking straight ahead.
 - 5. Subject's head was rotated to the right and flexed downwards.
- 6. Subject's head was rotated to the right and hyperextended upwards.

All of the above head/neck postures were voluntary maximum head/neck movements without discomfort to the subject. While flexing and extending at the neck, the subject was requested not to shift his original seated posture and try to keep his upper torso in the same position.

Forearm/Hand Study

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For this phase of the study, the subject was requested to remain seated centrally on the seat. The hand controller's lateral location was adjusted and locked at 9" to the right of the sagittal plane passing through the SRP. The subject gripped the handle in his right palm and the controller was moved so that (i) the elbow was just touching the back rest and (ii) the forearm was horizontal. The hand controller was fixed in this position, denoted as reference position, and the x (fore-aft) and z (up-down) coordinates of the hand controller were recorded. One set of pictures were taken with the subject holding the controller and looking straight ahead. The hard controller was then adjusted to positions 2 through 6 in sequence and a set of photographs was taken for each controller position while the subject was grasping the controller. Figures 11a and 11b show the different positions adopted for hand control position under different seat configurations. The hand controller was always displaced 9" laterally to the right of the mid-sagittal plane. However, the x and z coordinates varies depending on the reference position which again was determined on the basis of elbow touching the back rest and the forearm being horizontal. Thus, the six locations for hand controller were adopted separately for each of the five seat configurations for any one subject.

Rudder Pedal Study

In the foot rest (rudder pedal) study three locations controller levels, relate to SRP, were studied. They were:

(i) 1" above SRP.

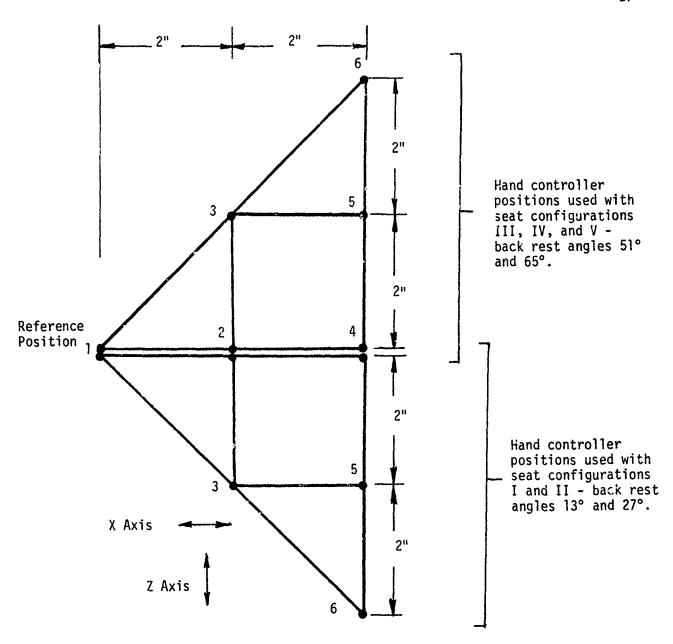


Figure 11 Controller Center Positions Adopted for the Five Seat Configurations

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- (ii) 1.25" below SRP.
- (iii) 3.5" below SRP.

These positions establish the location of the horizontal planes through the axes of rudder pedals. The left foot control was maintained at 6" farther away in front of SRP compared to right rudder pedal. This was done in order to simulate maximum SRP-to-pedal distances to the two extreme positions, assuming a 6" throw (range) for pedal travel. The subject was required to be seated all the way back on the seat and to rest his left foot on the left rudder pedal and push it all the way out as far as he can by extending the leg at the knee. The subject was instructed not to shift his seated position or bend forward during this maneuver. The rudder control platform was then locked in this position with a pair of setscrews. The neutral position of rudder controls (i.e., the mid-point between right and left rudder controls) along x axis was measured from SRP and recorded. The right rudder was then placed on the right foot pedal in a comfortable position. Next a set of pictures was taken with the subject looking straight ahead and resting his feet on the rudder pedals.

Data Reduction

The exposed film was processed at the Technical Photo Branch at Wright-Patterson Air Force Base. The processed film was projected through the digitizing system at AMRL/HED facilities and the specific coordinates of the selected body landmarks were punched on paper tape. This was later converted to real world coordinates with respect to the standard right hand coordinate system with the SRP as the origin.

Body landmarks 1 through 11 were identified with the help of suitable targets. Landmarks 12, 13 and 14 were not identified with any visible

targets, but rather these points were identified in the photographs in the following manner:

Landmark 12 - The rear-most point on the helment.

Landmark 13 - The body surface point about the thoracic vertebral region at which separation between the body and the upper back rest occurs.

Landmark 14 - The body surface point over the lumbar region at which maximum separation between the body surface and the back rest can be observed. (See Figure 12).

The positions of these 3 landmarks on the projected image were determined based on the judgement of the data reduction analyst. Figure 12 shows the location of these landmarks as defined above.

RESULTS

Engineering/anthropometric data generated from this study are presented in three separate sections:

- (1) Head/upper torso data,
- (2) Hand/arm rest data,
- (3) Foot rest data.

Head/upper Torso Data

This part of the study was performed to collect data pertinent to the design of the head rest. Figures 13 through 18 show the spatial locations of nasion, acromion, upper-back-contact point with back rest and the rear most point of helmet under each of the five seat configurations. (See page 35). Points 1, 12 and 13 are generally expected to be along the midsagittal plane of the subject. It can be noticed in these figures that

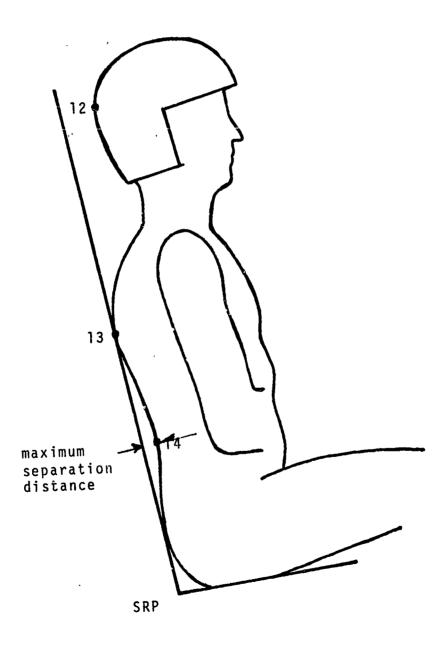
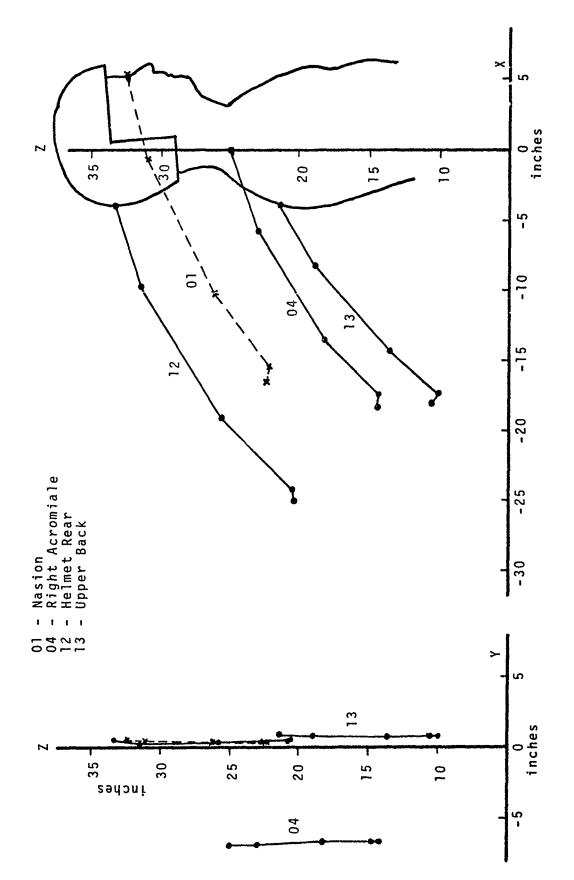


Figure 12 Locations of Landmarks 12, 13, and 14 With Respect to Seat Reference Point

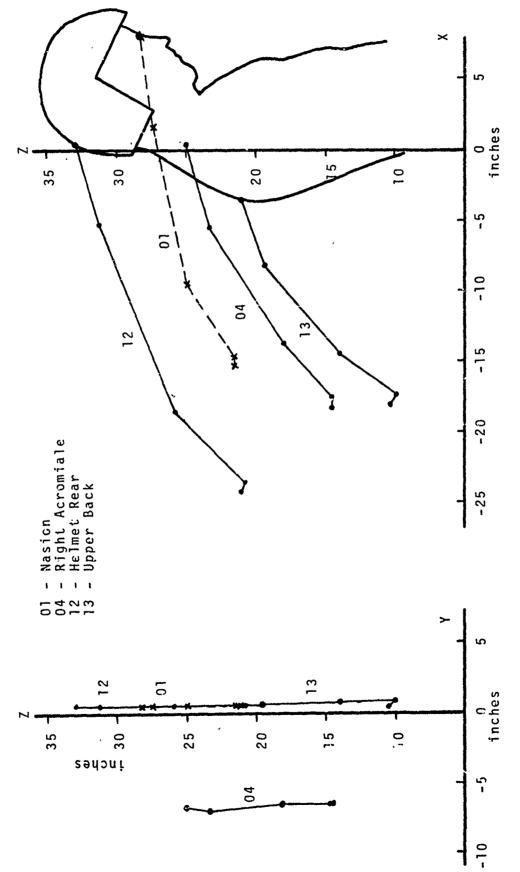
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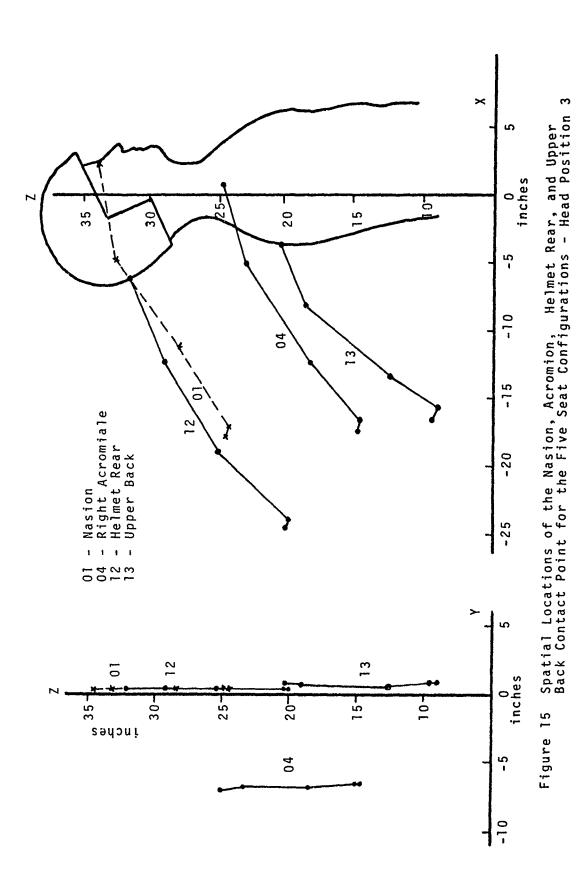


Spatial Locations of the Nasion, Acromion, Helmet Rear, and Upper Back Contact Point for the Five Seat Configurations - Head Position Figure 13

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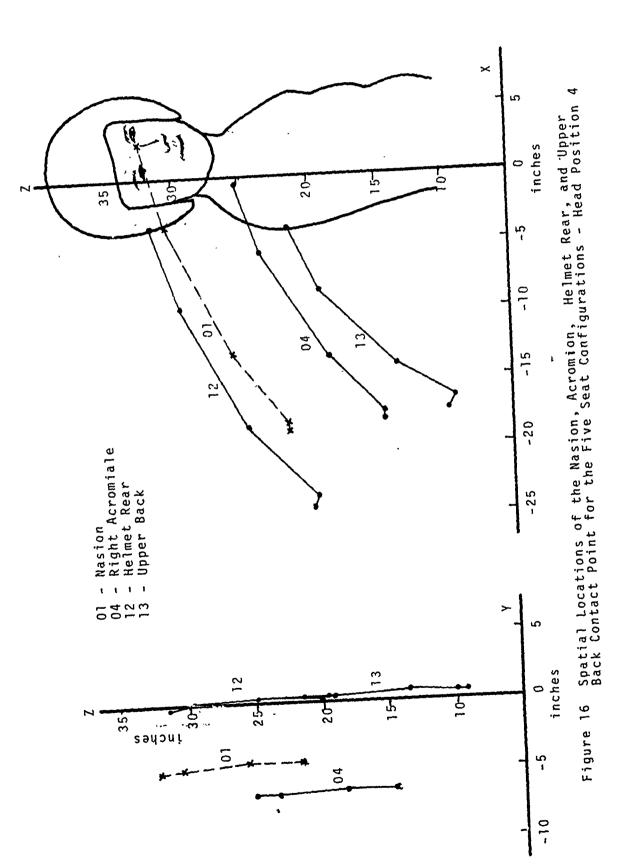


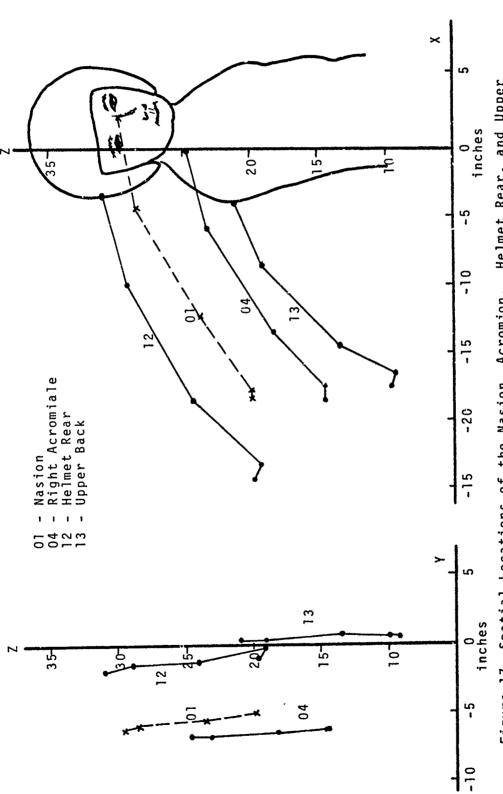
Spatial Locations of the Nasion, Acromion, Helmet Rear, and Upper Back Contact Point for the Five Seat Configurations - Head Position 2 Figure 14



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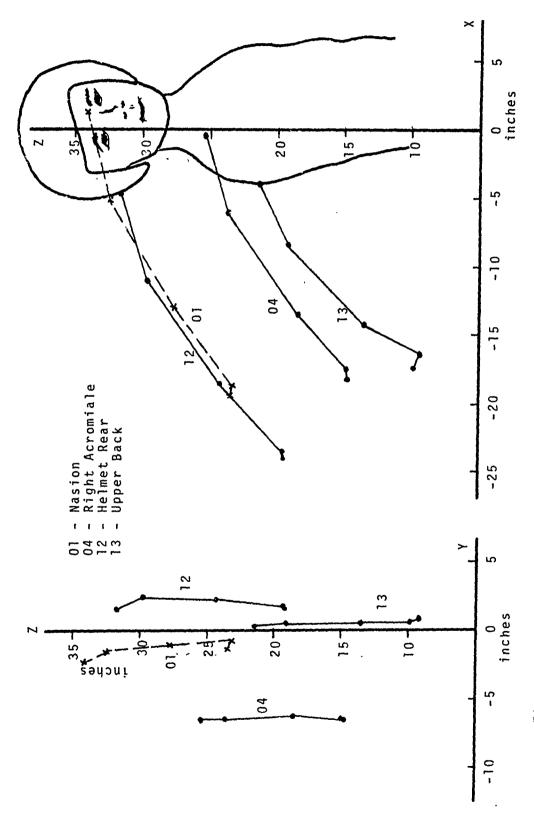
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Spatial Locations of the Nasion, Acromion, Helmet Rear, and Upper Back Contact Point for the Five Seat Configurations - Head Position 5 Figure 17

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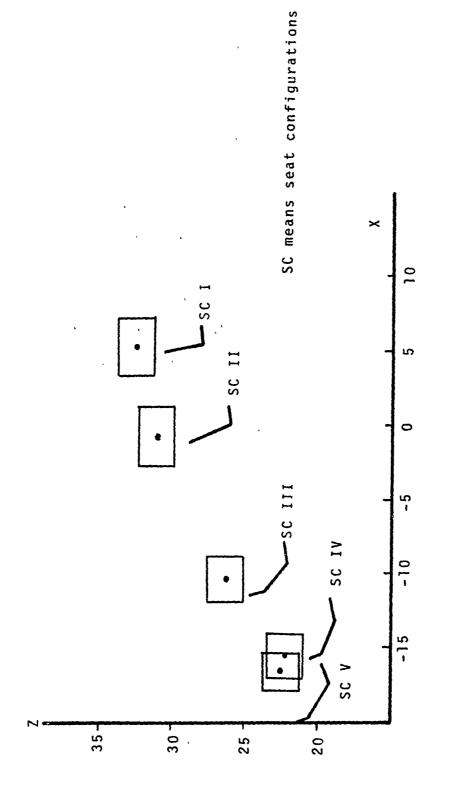
Spatia! Locations of the Nasion, Acromion, Helmet Rear, and Upper Back Contact Point for the Five Seat Configurations - Head Position 6 Figure 18

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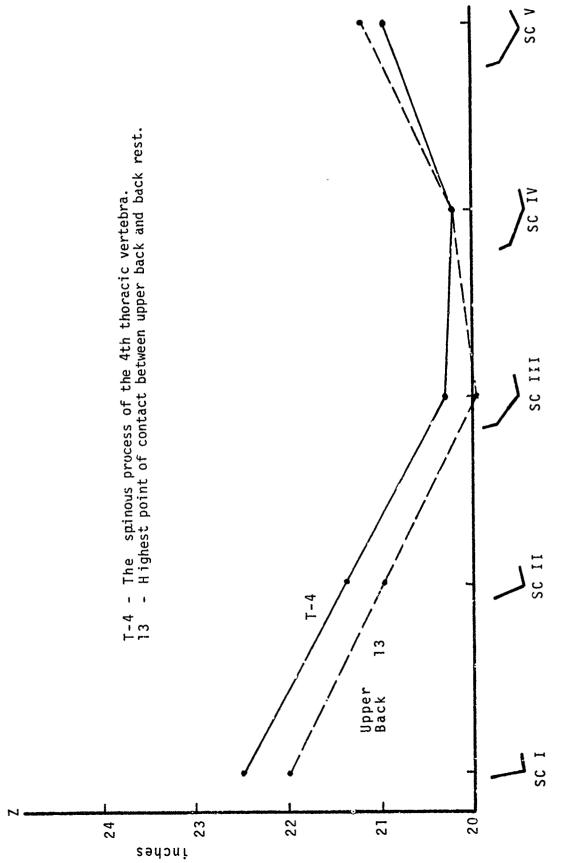
their locations along x and z axes change with the seat configurations. As expected, no appreciable changes were observed with regard to the position of these landmarks along the y axis. Between configurations IV and V, a change of 10° in seat pan angle results in a change of about 1/2" in locations of the points mentioned above. It must be remembered that the landmarks, "helmet rear" and "upper back," are not fixed anatomical points. Their positions are altered with changes in seat geometry. Appendix A-1 contains the same data presented in Figures 13 through 18 in a tabular format. In additions these tables also show the standard deviations for each data point. Figure 19 shows the nasion coordinates alone for the five seat configurations studied. The location of the mean, the 5th and 95th percentile limits in the mid-sagittal plane are shown. It should be noticed that in seat configurations I and II, the range of the nasion location is wider along the x axis than in the other three seat configurations. This is because the head rest was not used in seat configurations I and II. But it was consistently used during configuration III, IV and V. Thus the subject had much more freedom to position his head under configuraions I and II than under the other three configurations. This information will be useful in determining the required movement of the seat in the forward and upward directions under a given configuration so that the eye position may be maintained the same as the standard 13° seat configuration. These data are also presented in Appendix A-1 in tabular format.

Figure 20 shows the distances of T-4 position and landmark #13 from SRP along the back rest. T-4 point is the skin surface mark which identifies the 4th thoracic vertebra at upright seated position. Point #13 is the body point of contact with the subject's back and the back rest. T-4 mark

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The 5th, 50th, and 95th Percentile Positions With Respect to SRP for Waison - Head Position 1. The rectangle represents the 5th and 95th percentiles for both axes. Figure 19



The Distance Between T-4 and Highest Point of Contact Between Upper Back and Back Rest, Measured Along the Back Rest Figure 20

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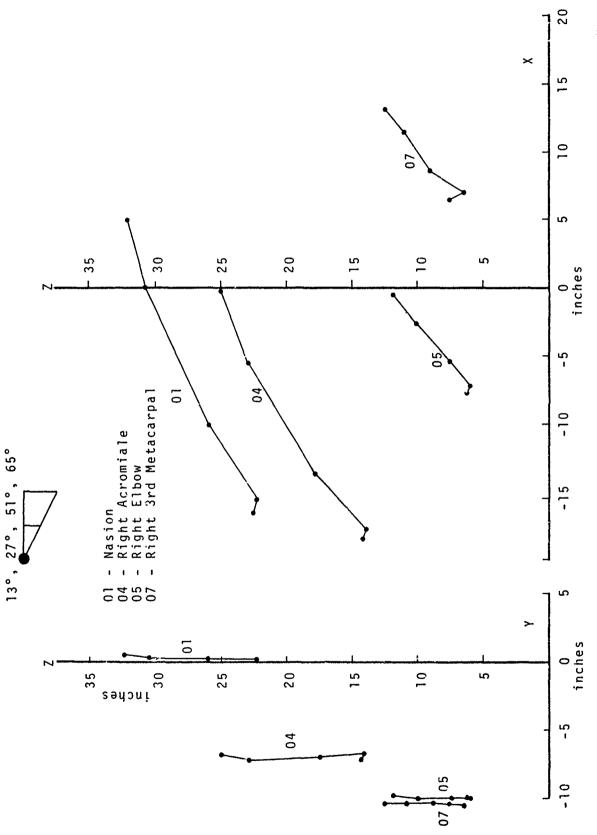
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is a fixed mark on body surface while landmark #13 may be changing with seat configurations. Under 13°, 27° and 51° back rest configurations, point #13 is below T-4 mark level. In other words, if point #13 can be taken as the hinge point for back rest, this hinge point can be located below T-4 surface mark for 13°, 27° and 51° configurations. However, at 65° back rest configuration point #13 and T-4 mark seem to coincide when the seat pan angle is 10°. But when the seat pan angle was raised to 20°, this shifted the entire upper body. Such a change resulted in moving the position of T-4 mark above landmark #13.

The data on locations of mention (point #2) and suprasternale (point #3) under different seat configurations and head positions are given in Appendix A-2. This information will be useful in determining the clearances available in the region forward of neck for purposes of possible interferences with face masks.

Hand-Arm Study

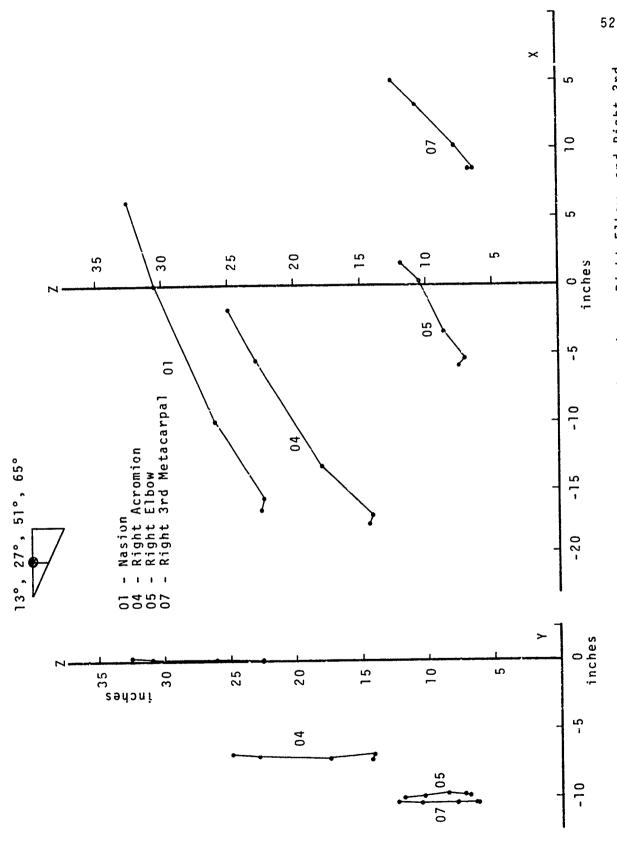
This study was performed to gather data on arm-hand configurations as a function of controller locations. These data will be useful in providing arm rest design parameters. Figure 21 shows the locations of nasion, acromion, elbow and third metacarpal joint for hand position 1 (i.e., the elbow in most rearward position against the back rest) under different seat configurations. Position 1 serves as reference and varies from subject to subject. Figures 22 through 26 show the same locations of nasion, acromion, elbow and third metacarpal for hand positions 2 through 6 respectively. It should be noted that hand positions 3, 5 and 6 were lower than hand position 1 for seat configurations I and II only. In the case of seat configurations 1!I, IV and V hand positions 3, 5 and 6 were



51 Spatial Locations of the Nasion, Right Acromion, Right Elbow, and Right 3rd Metacarpal for the Five Seat Configurations - Hand Position l Figure 21

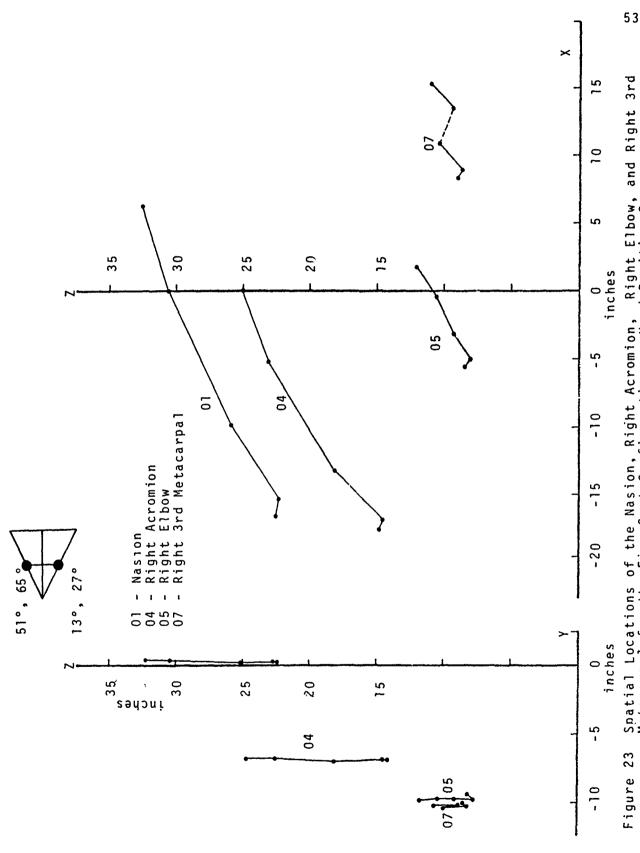
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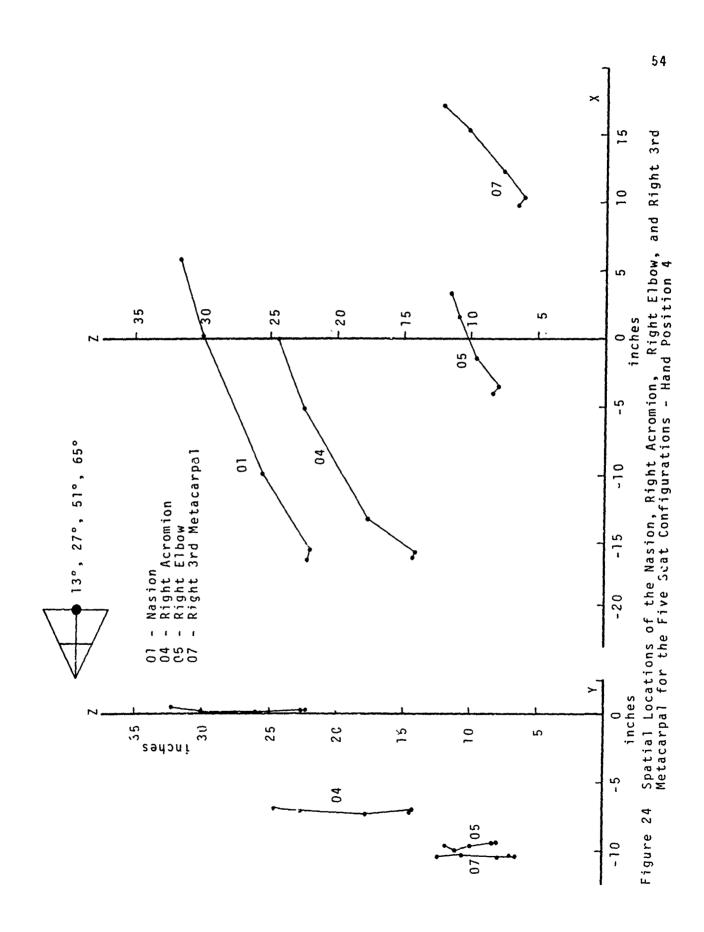


Spatial Locations of the Nasion, Right Acromion, Right Elbow, and Right 3rd Metacarpal for the Five Seat Configurations - Hand Position 2 Figure 22

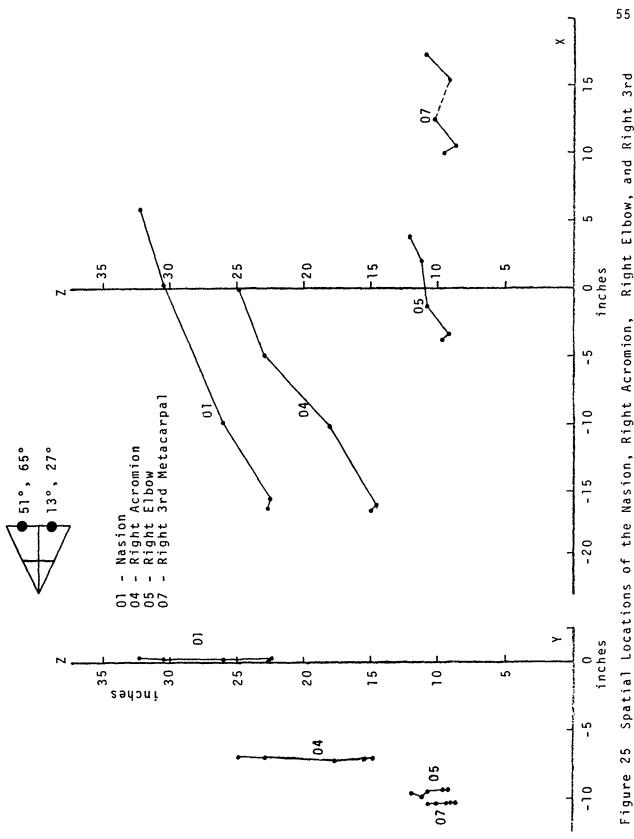
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Spatial Locations of the Nasion, Right Acromion, Right Elbow, and Right 3rd Metacarpal for the Five Seat Configurations - Hand Position 3

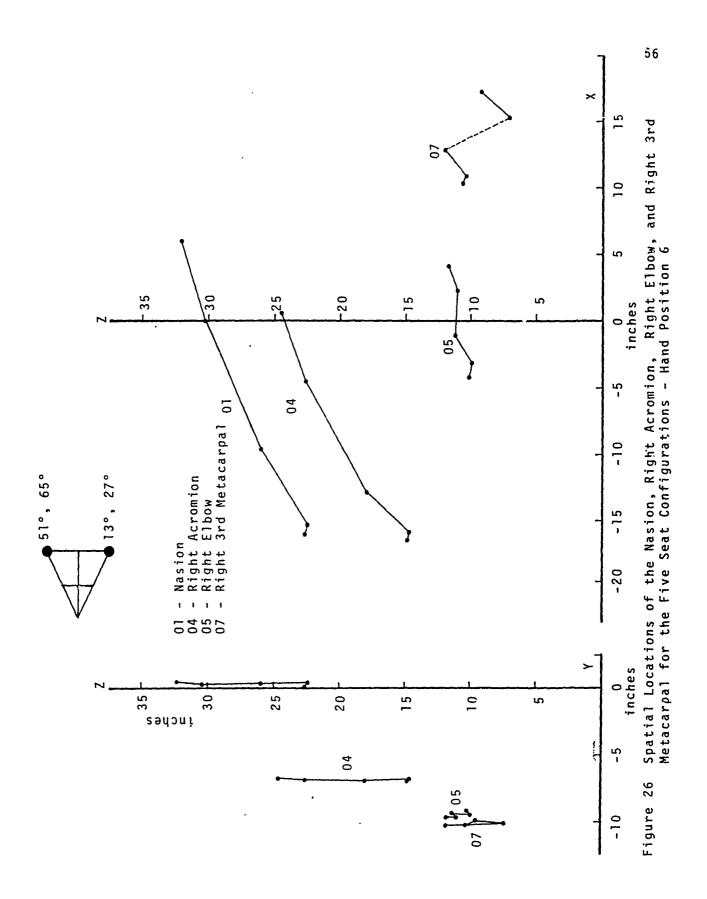


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Spatial Locations of the Nasion, Right Acromion, Right Elbow, and Right 3rd Metacarpal for the Five Seat Configurations - Hand Position 5

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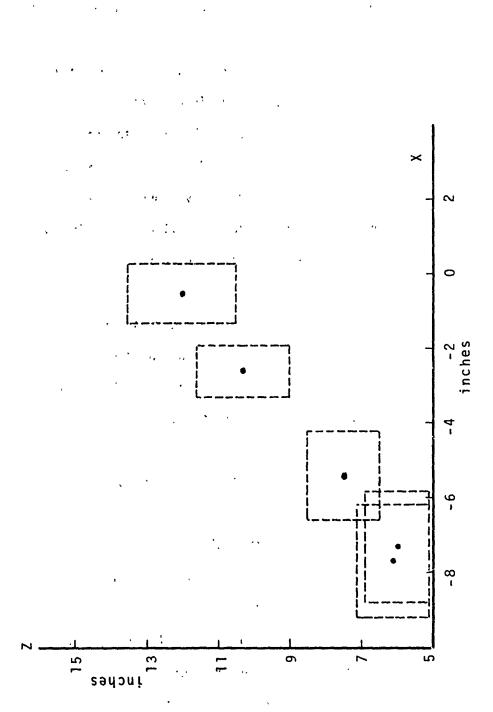
higher than position 1. The legend shown in each of these diagrams would be of help in noting this. The information shown in these figures is also presented in Appendix A-3.

Figure 27 shows the mean elbow locations along with the 5th and 95th percentile limits for hand position 1 under the different seat configurations.

The same data are also provided in Appnedix A-3. This set of data is useful in determining the forward location of a hand control because any location of the controller rear of hand position 1 may cause the back rest to interfere with elbow movement and hence controller activation. Figure 27 also shows relative shift in the elbow locations under the five seat configurations.

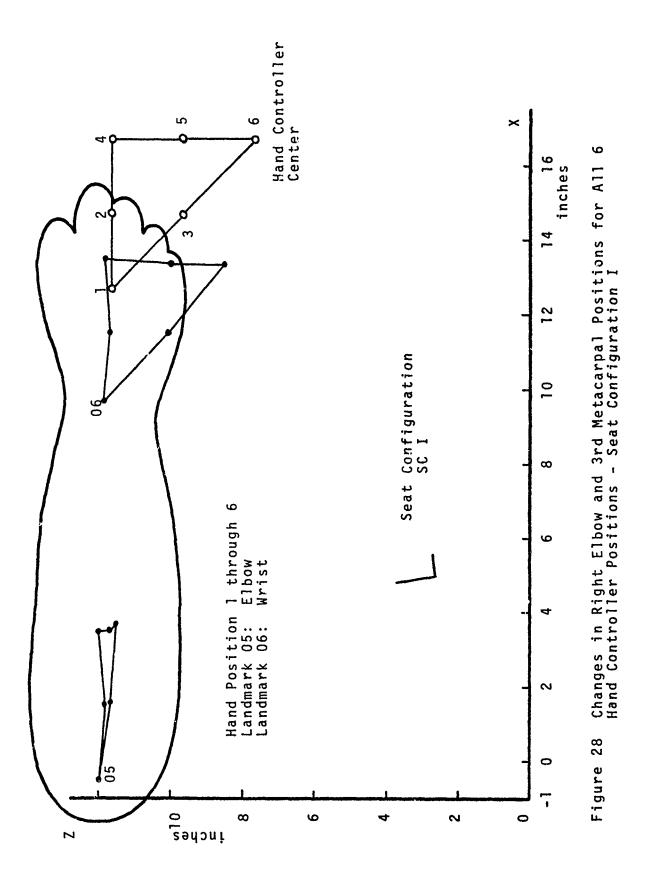
Figures 28 through 32 show the change in elbow and wrist locations for changes in controller positions under each of the given seat configurations. These data are useful in establishing the orientation and length of forearm support. As can be seen in Figures 28 through 32, the vertical displacements of the elbow for different controller positions are small for upright seated positions and are considerably larger for reclined positions.

Figures 33 and 34 show the mean locations of the hand controller along the x and z axis. Broken lines are used to indicate the effect of change in selecting hand controller positions for upright (13° and 27°) and reclined (51° and 65°) back rest configurations. Table 5 gives the mean locations along with the standard deviations for hand controller position under the five seat configurations. It must be remembered that the lateral location of the hand controller was fixed at 9" to the right of the SRP.

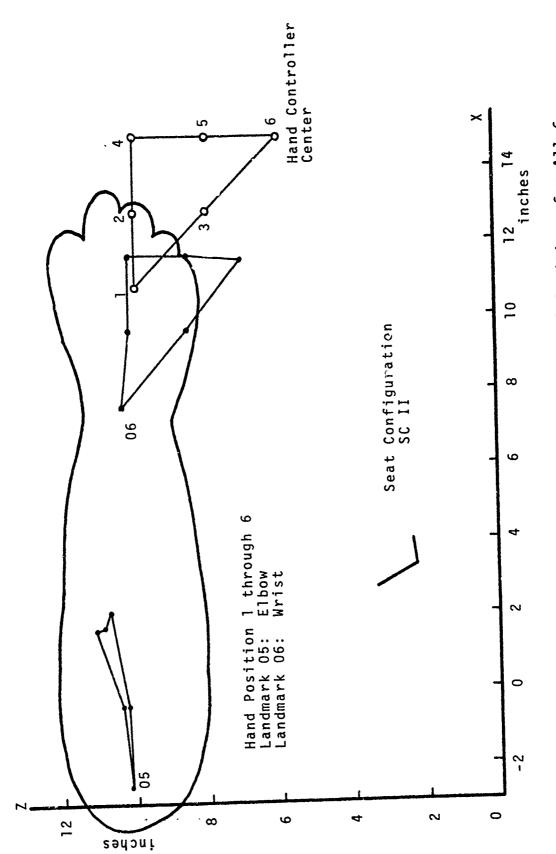


5th, 50th, and 95th Percentile Positions Above SRP the Elbow - Hand Position 1. The rectangle represents 5th and 95th percentiles for both axes. The for the Figure 27

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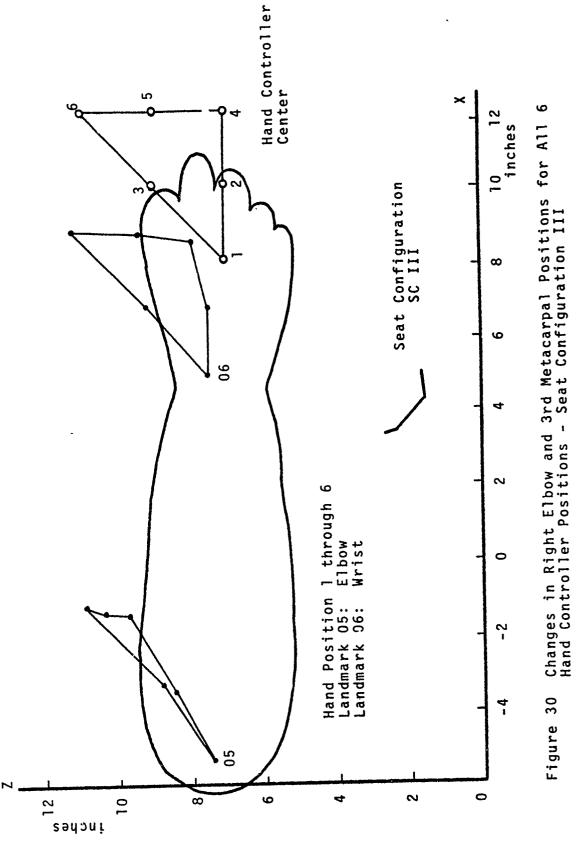


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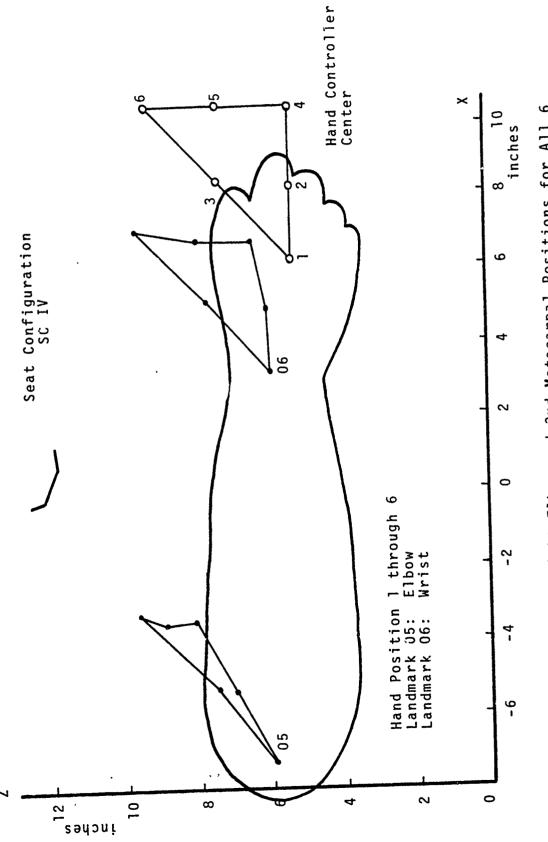


9 Changes in Right Elbow and 3rd Metacarpal Positions for All Hand Controller Positions – Seat Configuration ${\bf II}$ Figure 29

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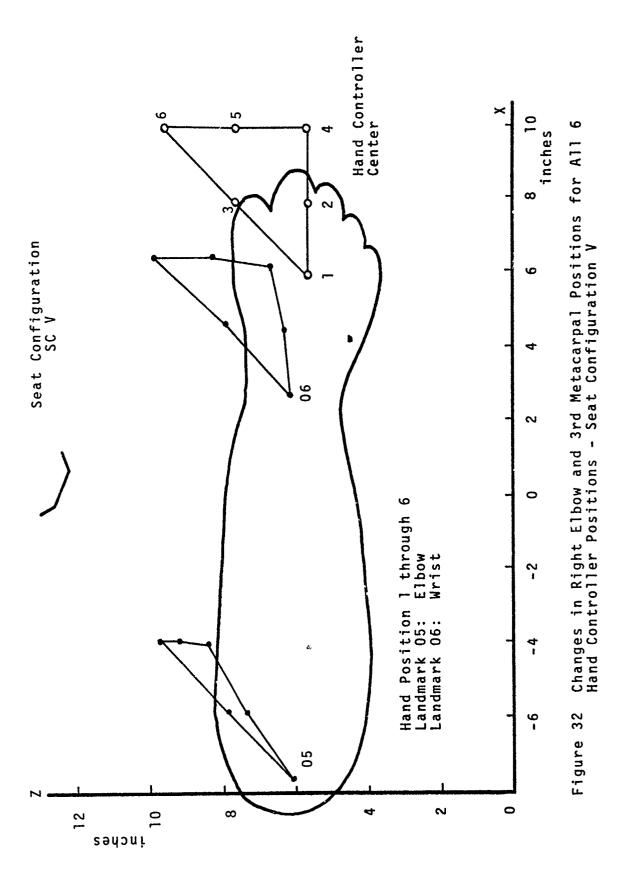
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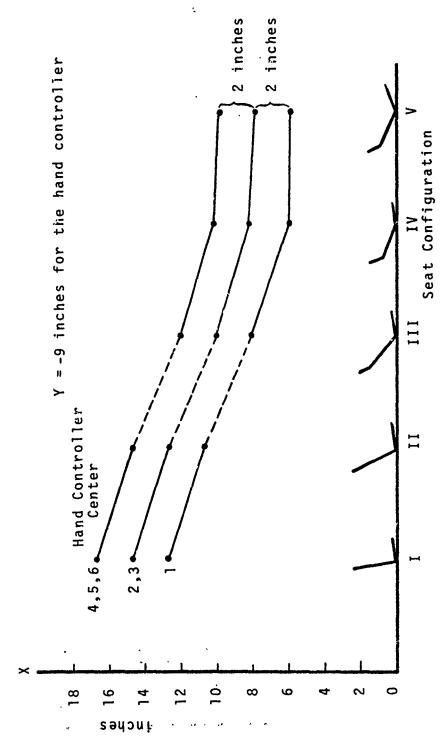


Changes in Right Elbow and 3rd Metacarpal Positions for All 6 Hand Controller Positions - Seat Configuration IV Figure 31

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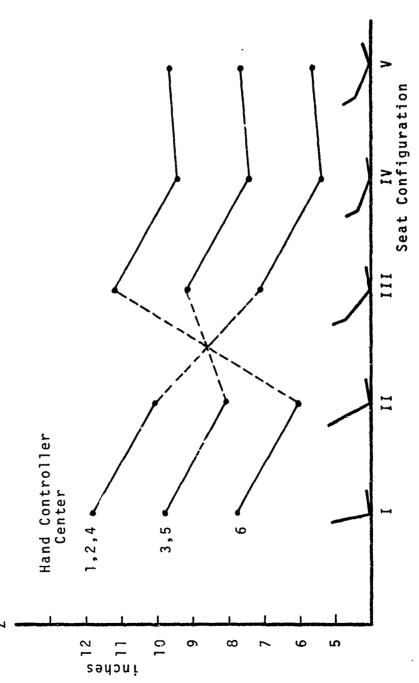




Distance of Hand Controller Center

Mean Location of the Hand Controller Center Along the X-Axis for All Seat Configurations Figure 33

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Mean Location of the Hand Controller Center Along the Z-Axis for All Seat Configurations Figure 34

TABLE 5
X and Z Coordinates for Controller
Midpoint Location*†

Seat			Hand Controller Positions**							
Config.	Coordinates	Statistics	1	2	3	4	5	6		
I	Х	Mean	12.68	14.68	14.68	16.68	16.68	16.68		
		Std. Dev.	0.68	0.68	0.68	0.68	0.68	0.68		
	Z	Mean	11.74	11.74	9.74	11.74	9.74	7.74		
		Std. Dev.	0.79	0.79	0.79	0.79	0.79	0.79		
11	Х	Mean'	10.85	12.85	12.85	14.85	14.85	14.85		
		Std. Dev.	0.76	0.76	0.76	0.76	0.76	0.76		
	Z	Mean	10.01	10.01	8.01	10.01	8.01	6.01		
	·	Std. Dev.	v.74	0.74	0.74	0.74	0.74	0.74		
III	X	Mean	8.07	10.07	10.07	12.07	12.07	12.07		
,	,	Std. Dev.	1.11	1.11	1.11	1.11	1.11	1.11		
	Z	Mean	7.13	7.13	9.13	7.13	9.13	11.13		
		Std. Dev.	0.61	0.61	0.61	0.61	0.61	0.61		
IV	X	Mean	6.29	6.29	8.29.	10.29	10.29	10.29		
		Std. Dev.	1.09	1.09	1.09	1.09	1.09	1.09		
	Z	Mean	5.38	5.38	7.38	5.38	7.38	9.38		
		Std. Dev.	0.47	0.47	0.47	0.47	0.47	0.47		
٧	X	Mean	5.92	7.92	7.92	9.92	9.92	9.92		
1		Std. Dev.	1.30	1.30	1.30	1.30	1.30	1.30		
	Z	Mean	5.72	5.72	7.72	5.72	7.72	9.72		
	1	Std. Dev.	0.47	0.47	0.47	0.47	0.47	0.47		

Y Coordinate was maintained at 9" right of SRP

⁺ Dimensions are in inches.

^{**} Hand positions varies from subject to subject.

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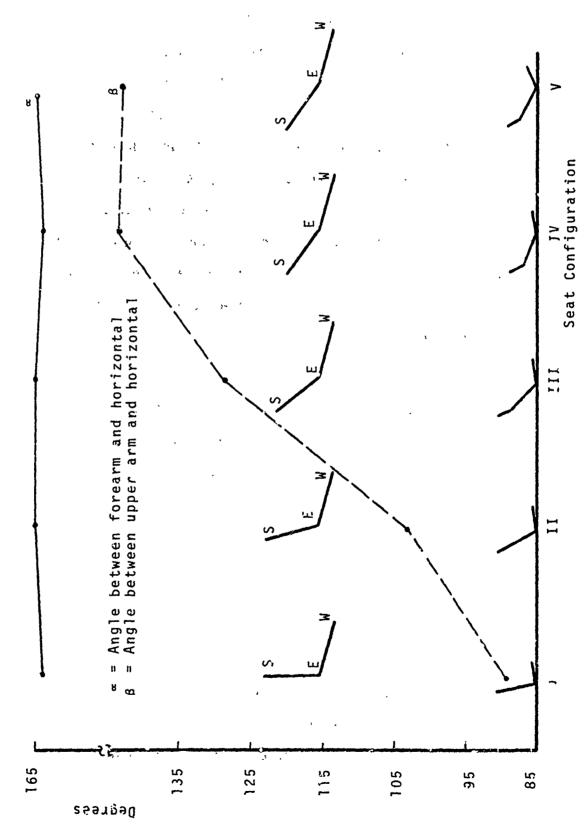
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When the back rest angle changes from the standard 13° configuration, the pilot's arm configuration is altered. These changes are in terms of the inclination of the upper and lower arms with respect to the x axis. Since arm configuration changes may influence the maximum isometric force exerted on the arm controller, it was decided to include these data in Figures 35 through 40 for future reference. In these figures, angle alpha (α) refers to the inclination of the straight line joining radiale and stylion to the horizontal. Angle beta (β) refers to the inclination of the straight line joining acromion and radiale to the horizontal. Thus, α provides information requiring forearm orientation and β provides information on upper arm orientation. These data are also presented in tabular format in Appendix A-4.

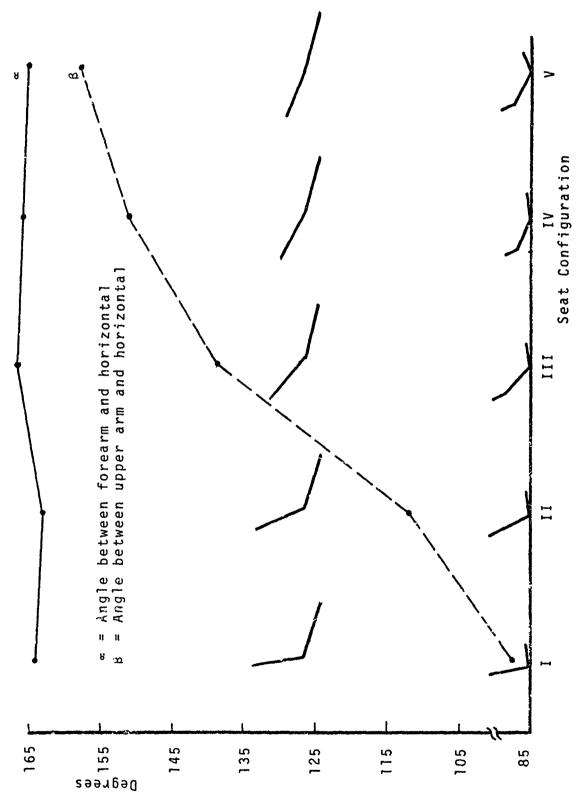
Foot Rest Study

The information on the average foot reach limit under different seat configurations and foot rest heights is presented in Figure 41 and also provided in the tables in Appendix A-5. This set of tables also gives information on the standard deviations for each reach.

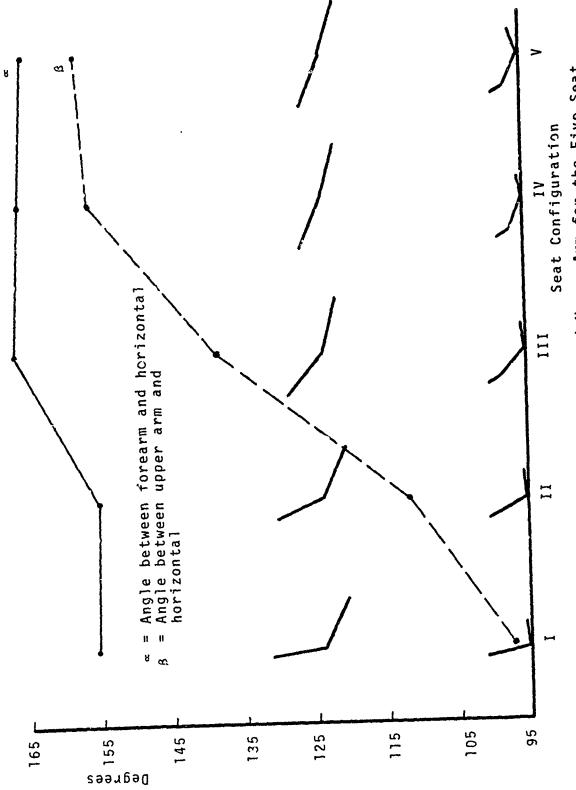
The information regarding visual interference with the knee was sought as a part of this study. Figures 42 through 45 show the mean locations of eye and knee top for the five seat configurations under three foot rest heights. Also shown are the mean locations of acromion and trachantion surface targets. Figures 26 and 47 show the relative displacements of knee top for change in seat configuration. These figures show the mean position and 5th and 95th percentile limits. The same data presented in Figures 41 through 47 also are presented in tabular form in Appendix A-5.



Mean Angles for the Forearm and Upper Arm for the Five Seat Configurations Measured From the Horizontal - Hand Position 1 Figure 35



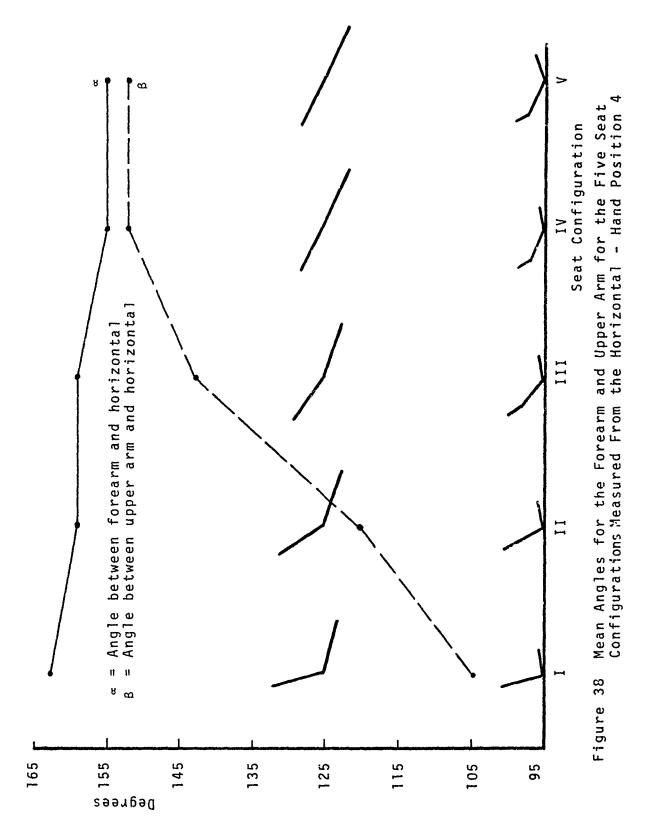
Mean Angles for the Forearm and Upper Arm for the Five Seat Configurations Measured From the Horizontal - Hand Position 2 Figure 36

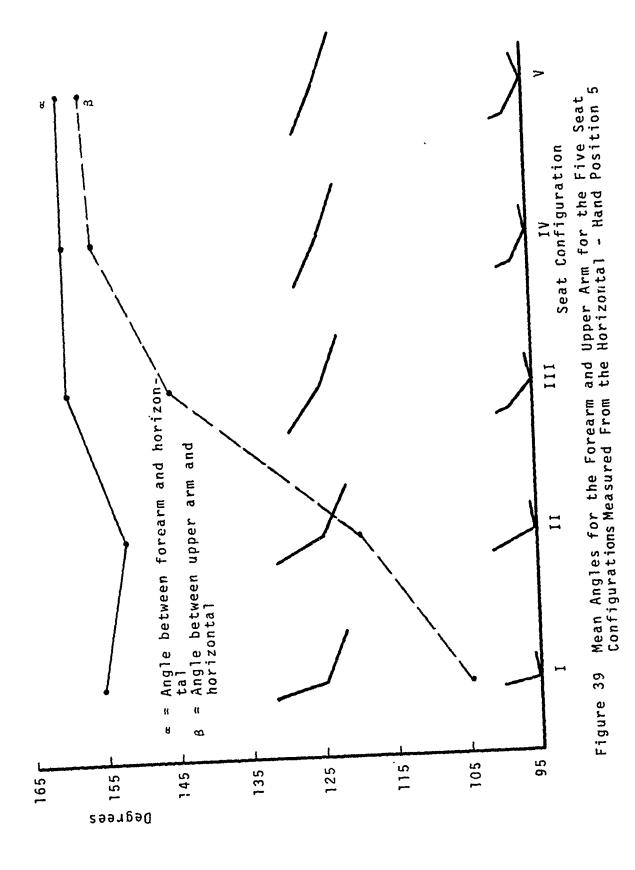


Mean Angles for the Forearm and Upper Arm for the Five Seat Configurations Measured From the Horizontal - Hand Position 3 Figure 37

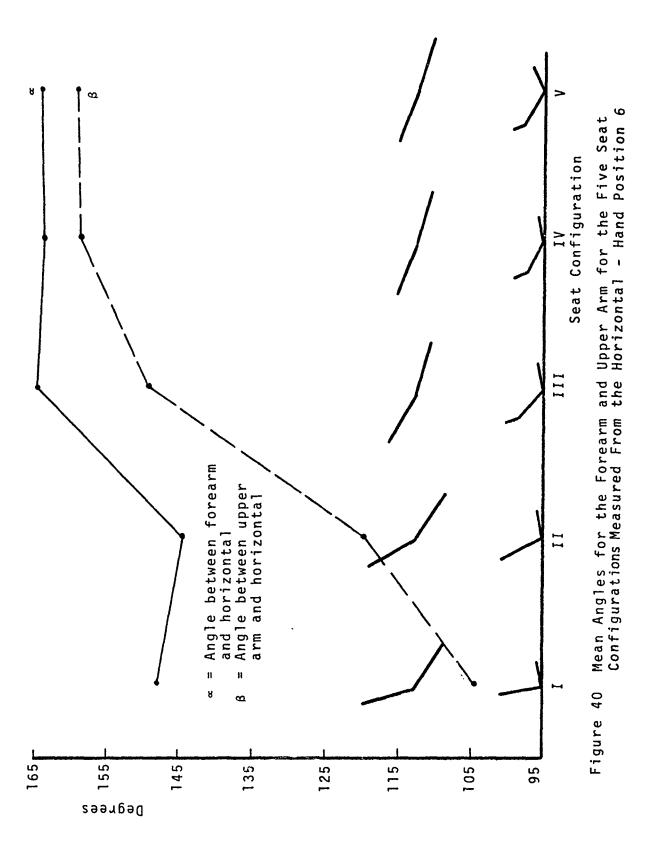
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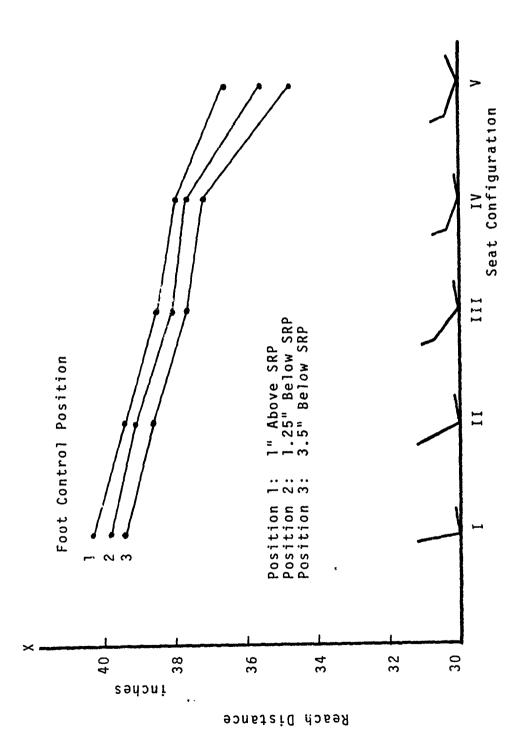




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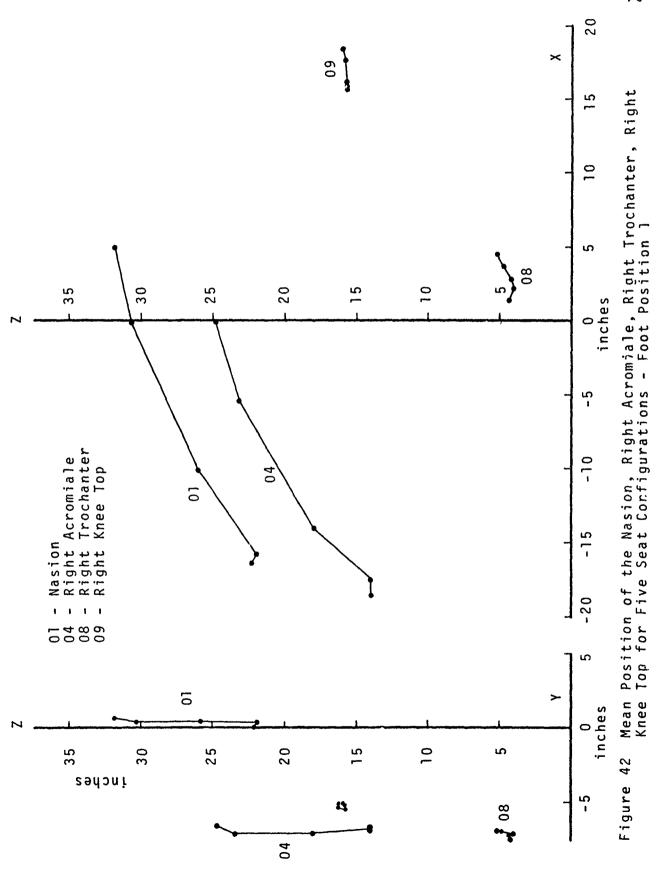


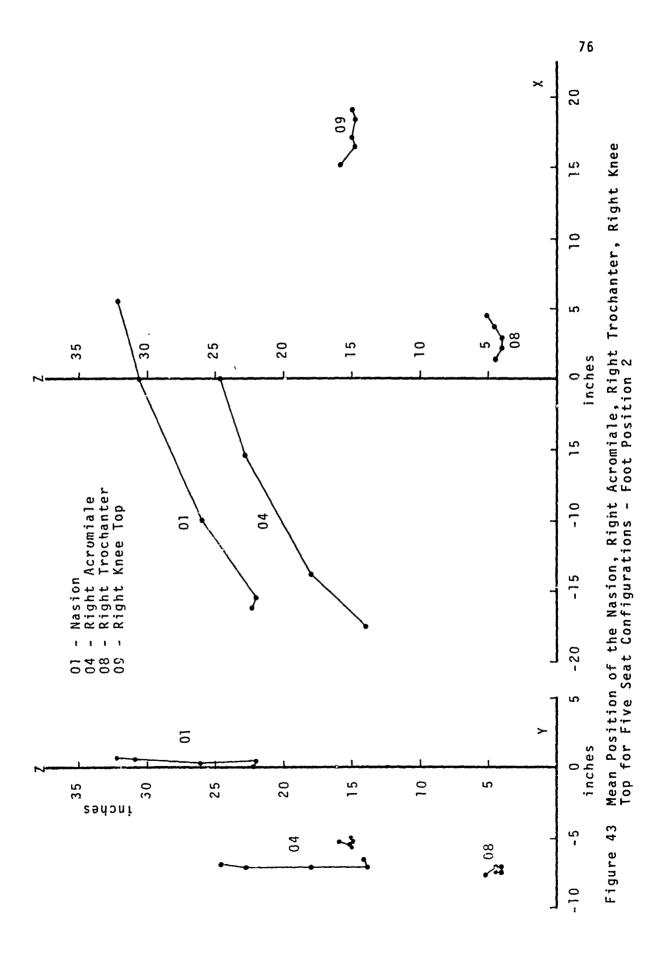
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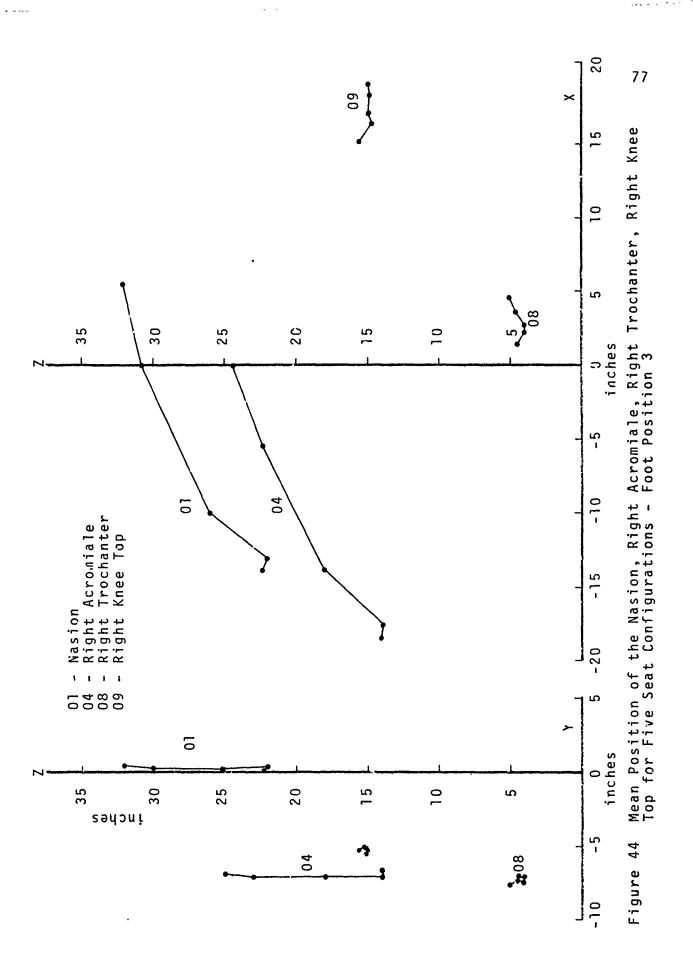
Average Foot Reach for Different Seat Configurations and Foot Control Location Figure 41

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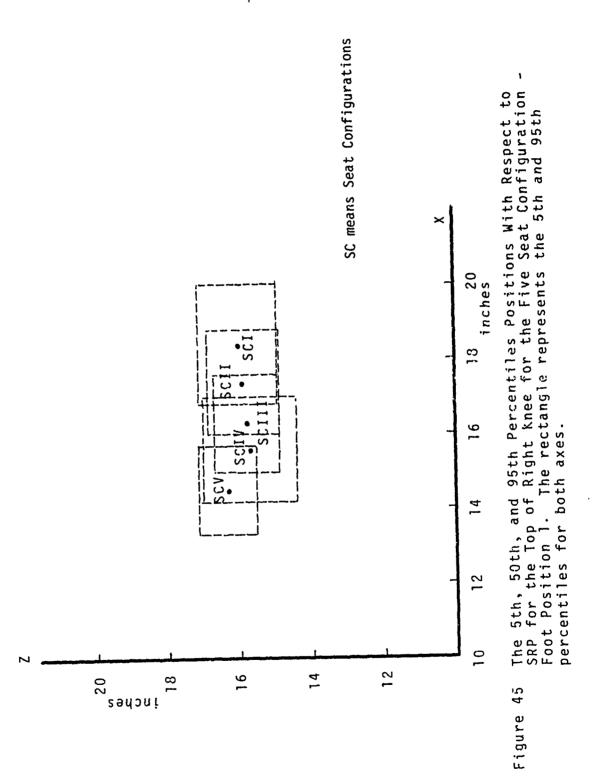


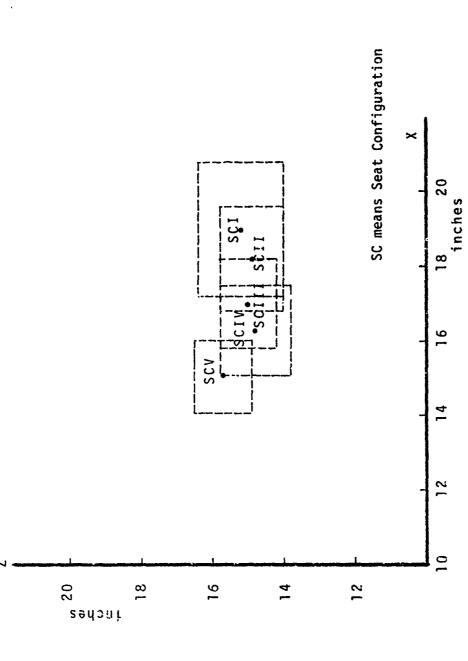
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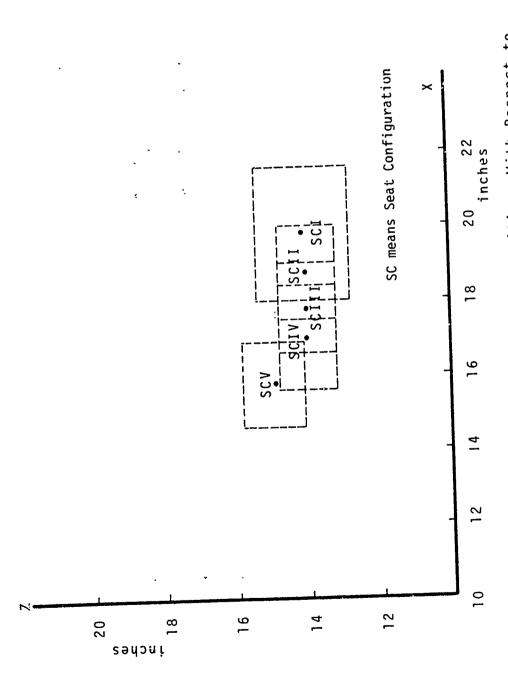
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The 5th, 50th, and 95th Percentiles Positions With Respect to SRP for the Top of Right Knee for the Five Seat Configuration Foot Position 2. The rectangle represents the 5th and 95th percentiles for both axes. Figure 46

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The 5th, 50th, and 95th Percentiles Positions With Respect to SRP for the Top of Right Knee for the Five Seat Configuration -Foot Position 3. The rectangle represents the 5th and 95th percentiles for both axes. Figure 47

CONCLUSIONS

The design conclusions based on the engineering anthropometric data collected are presented in four sections. These are: head rest, arm rest, foot rest, and eye design height which influences the position of the SRP as the seat reclines from the standard configuration (13° back angle) to the 65° back angle.

Head Rest

To adequately design a head rest, a minimum of two parameters are needed. These are the location of the hinge point and the length of the head rest.

The location of hinge point for the back rest is most difficult to obtain accurately. However, based on the data presented in Figure 20, the highest point of contact of the torso with the back rest ranges around the level of the spinous process of the fourth thoracic vertebra. Therefore, it may be assumed that the hinge point for the back rest should be at the same location on the back rest as the supinous process of the fourth thoracic vertebra. It should be noted that the head rest is not used for seat configuration I, II (back rest angles 13° and 27°).

The length of head rest based on the data shown in Appendix A-1 should be approximately 15.84 inches. This represents the distance for 95 percentile (based on the subject population used) from the hinge point to the helmet rear contact point. This value is based on head position 3 for seat configuration V which requires the longest head rest among all head position - seat configuration combinations.

Arm Rest

The arm rest parameters of interest in this study were:

- 1. Location of arm rest.
- 2. Orientation of the arm rest.
- 3. The change of orientation of arm rest as the back rest reclines for a given controller location.

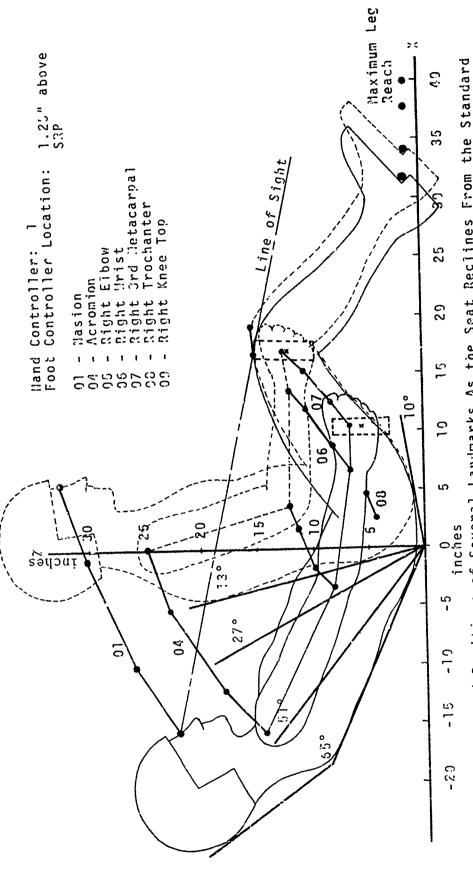
Figures 29 through 32 show for a given location of the hand controller, the position of the desired seat configuration. These data, also available in Appendix A-4, provide the needed information to establish the expected position of the arm-rest in space. In addition they give the relative change in orientation as the seat reclines from the standard seat configuration (SCI) to seat configuration IV (65° back rest, 10° seat pan). This is illustrated in Figure 48 which shows the spatial histories of several landmarks as the seat reclines.

To obtain the arm configuration during reclining of the seat, Appendix A-4 provides the tabulated data for the elbow and wrist positions from which the arm rest orientation during reclining of the seat can be determined.

Foot Rest

Three foot rest locations were used to establish maximum reach as well as the position of the knee when the seat is fully reclined. The data obtained give information on the line of vision of the pilot in the various seat configuration to the top of the knee. These data, given the location and dimensions of the instrument panel, can define the areas of the panel that are obstructed to view by the pilot's knees in the different seat configurations.

The maximum reach data give the design limit for location of the foot controls forward of the seat reference point along the X-axis.



The Expected Positions of Several Landmarks As the Seat Reclines From the Standard Seat Configuration (SCI) to Seat Configuration Naving the Back Rest at 65° and Seat Pan of 10°(SCIV) Figure 48

Table 6 gives the maximum foot reach measured from the mid position of foot controllers.

Eye Design Position

Because of the reclining seat configurations, the eye position moves both backward and downward as the back rest is reclined. Therefore, in order to maintain the eye position the same, the seat reference point (SRP) must be repositioned in order that the eye position is maintained the same.

Table 7 shows the x-z coordinates for the SRP for the standard as well as the other seat configurations for the 5th, 50th and 95th percentiles of the 9.S. pilot population. From these data the needed SRP translations along the x and z axes have been computed and are also shown in Table 7.

TABLE 6

Maximum Foot Reach Measured from the

Mid Position of Foot Controllers

Seat C	onfigurat	ions	I	II	III	IV	<u> </u>	
	1	- x	40.29	39.41	38.47	38.01	36.55	
	<u> </u>	σ	1.42	1.35	1.30	1.34	1.63	
Position			· · · · · · · · · · · · · · · · · · ·					
s i t	2	x	39.75	39.14	38.06	37.66	35.63	
		σ	1.42	1.47	1.28	1.35	1.53	
Foot								
LL.	3	x	39.38	38.60	37.72	37.17	34.75	
		σ	1.37	1.49	1.32	1.47	1.56	

Note: (i) Distances are in inches.

(ii) Controller maximum travel is 6 inches.

TABLE 7

Translation of SRP required to maintain the eye position of Head position I, SC I, for 5th to 95th percentile (±1.65 std. dev.).

		SE	SEAT CONFIG	CONFIGURATION		
COORDINATES	1	II	III	ΛI	Λ	Percentile
>	~ (4,	-8.6	13.9	5.	95
<	3.38	-2.82	-10.21	-15.63	-16.46 -17.75	
•	3.8	2.1	7.3	3.5	3.	95
4 1	32.53	30.90 29.63	26.20 25.09	22.31 21.07	22.47 21.26	+50th + 5th
TRANSLATION				1	1	
\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \		.7	ις,		31	95
6 K & & & & & & & & & & & & & & & & & &		5.37	15.14	20.66	21.13	+50th + 5th
		9	•	0.2	0.1	95
Along Z axis		ယ္		0.2	1.2	→50th
		9.	•	0.	ο.	3

*Distances are in inches.

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- Kulwicki, P.V. and J.M. Sinnett. The High G Approach. AMRL-TR 73-27.
 Aerospace Medical Research Laboratory, Wright-Patterson AFB, Dayton,
 Ohio. [Also MDC A2109, McDonnell Aircraft Co.] [AD 757216]
- 2. Dept. of Air Force. Physiology of Flight, AF Manual 160-30.
- 3. National Aeronautics and Space Administration. Bioastronautics Data Book, second ed., 1973. NASA SP. 3006. NASA, Washington, D.C.
- 4. Gell, C.F. and H.N. Hunter. Physiological Investigation of Increasing Resistance to Blackout of Progressive Backward Tilting to the Supine Position. The Journal of Aviation Medicine, 1954, Vol. 12, 568-577.
- Crossley, R.J. and D.H. Glaister. Effect of Posture of Tolerance to Positive (+G_Z) Acceleration. Adaptation and Acclimitization in Aerospace Medicine, H.J. Grunhofer (Ed.) AGARD, CP 82-71, March, 1971.
- Von Beck, H.J. Protective Tilting Aircraft Seats. NADC-72-063-CS, March, 1972.
- 7. Replogle, C.R., et. al. Manned Weapon Systems Effectiveness in High Performance Aircraft. Presented at the Review of Air Force Sponsored Basic Research in Environmental and Acceleration Physiology, Wright-Patterson AFB, Ohio, Sept. 1973.
- 8. Sinnett, J.M. and C.F. Asiala. Advanced Fighter Concepts Incorporating
 High Acceleration Cockpits. Vol. IV--Pilot Performance Analysis.

 AMRL-TR-72-116. Wright-Patterson AFB, OH. [AD 913694L]

- 9. Von Beck, H.J. Biomedical Considerations for the Development of a PALE (Pelvis and Legs Elevating) G Protective Aircrew Seat. Paper presented at the Conference of Aerospace Medical Association, 1973, Las Vegas, Nevada.
- 10. Sinnett, J.M. and L.N. Edginton. Advanced Fighter Concepts Incorporating
 High Acceleration Cockpits. Vol V--Crew Station Concepts. AMRL-TR-72-117.
 Wright-Patterson AFB, Ohio. [AD 913695L]
- 11. Leverett, Jr., S.D. Acceleration Capability Enhancement. Medical Service Digest, February, 1974, 13-16.
- 12. Rogers, D.B., et. al. Effect of Modified Seat Angle on Air to Air Weapon System Performance under high Acceleration. AMRL-TR-73-5.

 Wright-Patterson AFB, Ohio. [AD 770271]
- 13. Kennedy, K.W. and K.H.E. Kromer. Excursion of Head, Helmet and Helmet Attached Reticle under G_Z Forces. AMRL-TR-72-127. Wright-Patterson AFB, Ohio. [AD 767201]
- 14. Ayoub, M.M., S. Deivanayagam, and Kenneth W. Kennedy. Paths of Movement for Selected Body Segments During Typical Pilot Tasks. Final Report AMRL-TR-75-111. Wright-Patterson AFB, Ohio. [AD A-025773]

APPENDIX A-1

Head/Upper Torso Data

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- Note: 1. All linear dimensions in the following appendices are specified in inches. Angles are specified in degrees.
 - 2. A blank space indicates that the specific data was not available.

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	Z-MEAN		***	4.6	0.7	6.	4.8	6.1	0.8	9.4	7	9.6	2.9	3.2	9.3	8.9	8.1	8.3	4.7	9.0	8.5	5.2	2.6	5.2	4.3	1.3	6.1	8	0.0	8.9	9	4.6	•	6,3	4.9	0.2	9.50	7.
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	Y-MEAN		**	m	ď.	S	Ģ	4	7.	3	•	4.	.7	8	3	3	8		4	4.	8	3	3	•	5	5	9.	•6	•	1.	'n	٣.	4.	3		ŝ	19.0	5
ы	۲,	VIAT	* * * * * * * * * * * * * * * * * * *	4	6.	1	0	0	.5	3	S	7.	1.	8	6	4.	'n	•	3	6.		8	8.	6.	-	6.	4	.2	ဆ	4.	.2	0	6.	0	i,	. 1	1.18	1.08
AD PGS IT	X-MEA		* * * * * *	.2	•	.2	S	7	9.	8	-	5		5.3	2.6	8.1	2.4	1.2	8.0	დ• ფ	2.5	8.9	13.4	3.9	17.1	3.4	13.0	1.9	4.1	15,8	1	17.9	4.4	13.6	5.2	24-8	-16.82	5.4
	SAMPLE	S12E	*	21	21	21	21	21	21	21	21	21	21	21	21	21	21	21	21	21	21	21	21	21	71	21	77	21	21	21	21	21	21				20	
1	POINT	Q	* * * * *	4	7	ო	4		13		-	7	m	4		13		-	7	M	4		13		rd.	7	m	4		13		4	7	m	4	_	13	-
1	SEAT PAN	ANGLE	***	10	10	10	01	07	10	10	10	10	10	10	10	10	01	. 01	10	70	10	70	07	10	01	10	10	01	10	10	07	20	20	20	20	20	20	20
1	BACK REST	ANGLE	**							m		F-4		_																							65	

more of the manufection of the second contract of the second contrac

	Z-STAND EVIATIO	***	5	6	9			•	-	-		•	8	6	8	8	8	ω.	'n		9	9		0.59	•	4	• 6	9	8	4.	9	-	4.	8	7	6.	1
	Z-MEAN	***	2.1	7.4	3.9	7	1.5	1.4	9.3	0.5	5.9	2.7	3.4	•	9.1	8.0	5.6	1.1	6.	8.3	4.7	3.4	5.3	21.71	7.4	5.7	4.4	9.6	9.3	0	1.7	.5	5.9	4.5	0.0	8	7.
	Y-STAND EVIAT 10	*	0	ę	4	4.	9	4.	ŝ	8	~	4.	ů	6.	4.	'n	6	8	4.	9	6	4.	u.	1.16	æ	~	0	3	•	Š	0	8	5	9.	o.	4	3
	Y-MEAN	****	4.9	8	4	•6	.2	4.	.7	4.6	8	ů	9	0	3	ů	7	4.	4.	4.	7.	-	ŝ	-3.89	3.3	ů.	•	0	ŝ	4	4.2	4.	0	•	0.2	Ą	5
4	X-STAN EVIATI	*	7.	Š	7.		4	4.	æ	•	4	8	8	•	4	in	0	6.		0	8	φ,	•	1.27	Ġ.	6.	•	ō	0	.2	4.	-	8	Ò	7.	7.	•
PCSIT	EA	****	4	8	5	9.	7.	•		ထ္	•	6.	۲.	•	4.	2.5	2.9	1.3	•	3.6	8.5	7	4.1	-18-17	15.7	3.6	4.7	23.7	9	4.9	18.8	4.	4.3	8.1	4.	7.5	5.
H	SAMPLE))	77	21	71	21	20	20	21	21	77	21	21	77	21	21	20	20	20	20	20	20	20	21	21	77	77	21	77	21	20	20	20	20	20	20	20
	POINT NO.	***	-4	2	m	4		13		7	7	ю	4		13		-	7	m	4	12	13	14	-1	7	m	4		13		7	7	m	4		13	
	SEAT PAN	****	01	10	01	10	10	07	70	10	07	07	01	07	10	10	70	10	10	70	10	01	07	10	10	10	10	07	01	01	20	70	20	20	20	20	20
	BACK REST ANGLE	****	13	13	13	13	13	13	13	27	2.7	2.7	27	27	2.7	27	51	15	15	51	51	51	51	9	9	65	65	9	65	65	65	99	99	65	65	65	65

	2-STAND DEVIATION	****	7	6	•	1.	8	0	1.	0.80	8	•	1.	6.	.7	6	•	1	'n	.7	0	6.	1	•6	S	4.	9	7	æ	4.	Ŝ	4.	4.	8	7	0	4.
	Z-MEAN	***	7.6	5.7	3.9	4.8	1.0	3	9.4	28.49	4.4	2.7	3.2	1.6	9.1	A.0	3.8	4.1	d • &	8.2	4.3	3.5	5.3	0.0	6.2	5.7	4.	9.5	~	4.0	0.1	٣,	5.9	4.4	1.6	8	7.
	Y-STAND EVIATIO	***	7	6.	9	5	0	9	. 7	1.06	6	1.	9	7	4.	4.	3	6	• 6	1.	0	S	4.	4	0	8	0	.2	S	4	7.	0	9.	8	~	4	.3
	Y-MEAN	****	6.3	9	0	6.8	0	4	6.	-6.10	3.6	7	^ •	9.	9.	•	5.3	5	Ą	S	1.1		ď	0	7.	3	7	8	'n	4.	5.2	7	7	4.	7.	3	ŝ
1 ON 5	X-STAND DEVIATIO	* * * *	0	4.	- 7	7	0	3	Š	2.17	4.		6.	1.	S	5	~	8	1.	0	6	8	0.	7	8	• 9	6	6.	6.	.3	.2	0	8	0	0	0	0
0517	X-MEAN	****	4		7	0.3	3.6	6.	0.9	61.4-	4.	7-7	5.8	0.0	8.3	2.5	12.2	1.2	9.6	3.6	4. B	4.2	4.0	17.8	5.5	3.5	'n	3.5	16.6	5.0	8.2	6.1	4.2	8.2	4.2	11.5	5.3
ш		* *	21	21	77	21	21	21	21	21	21	21	21	77	21	21	21	21	21	21	21	21	21	21	21	21	21	21	21	21	21	21	21	21	21	21	17
	POINT NO.	***	-	7	m	4		13		-	7	m	4		13		7	7	m	4		13		7	7	m	4		13		~	7	m	4		13	
	SEAT PAN ANGLE	**	10	01	10	07	01	01	01	10	10	07	07	01	70	10	01	01	07	10	01	07	07	01	10	10	07	10	01	01	20	20	20	20	20	20	70
	BACK REST ANGLE	***	13	13	13	13	13	13	13	2.7	7	. 12	27	27	27	~	51	51	15	21	51	51	15	65	9	65	65	99	65	65	65	99	65	65	65	65	65

Z-STAND DEVIATION ******	0	"	0.70	8	7	0	7	8	0	•	8	•2	ٿ	0	æ	•	S	9	.7	0		. 7	0	4.	1	8	æ	4	8	0	4.	8	0	7	r.
2-MEAN	4.2	9.8	24.09	5.4	1.7	1.5	4.6	2.5	8.2	2.9	3.8	.7	9.3	8.2	7.6	3.5	9.0	8.5	4.	3.6	5.3	.3	9.7	5.9	4.7	9.5	7.	3.9	3.3	9.7	7.	4.7	9.8	8	• 2
Y-STAND DEVIAT ION ******	4	6	0.68	3	'n	7.	3	6	6.	'n	3	٠,	4.	4.		ń	Š	•	'n	5	3	æ	7.	9.	•	ż	9.	3	9	0	3	•6	4.	ŝ	• 3
Y-MEAN	2.1	S	0.18	9.	4	3	7	1.5	6.	3	4.	6.	4.	•6	6.	'n	3	.3	.2	9.	•	9.0	4.	4.	4.	8	••	ů	1.1	5	J.	4.	٠,	•	3
0 ND I ON STATE OF THE PROPERTY OF THE PROPERT	-2	5	0.74	Š	2	4.	2		. 7	8	8	. 7	4.	•	4.	7	. 7	•	4.	8	7.	5	0	• 9	6.	8	0	7.	7.	•	8	0	•	~	~
AD PCSITI X-MEAN *****	7	20	3.29	0.4	9	6	6.0	5.2	7,	6.	5.0	0.8	8.4	2.5	6	6.0	9.3	3.6	18.3	14.2	4.1	18.7	16.0	13.4	7.5	23.7	16.3	4.8	19.4	16.7	14.1	18.2	4.2	17.5	5 •6
HE. SAMPLE SIZE *****	21	21	21	21	21	21	21	20	20	20	20	20	20	50	21	21	21	21	21	20	21	21	21	21	21	21	21	21	20	20	20	70	20	20	70
PO INT NO. **	-	· ~	ı m	4			71		7	M	4		13			7	m	4		13			7	m	4			14		7	æ	4		13	
SEAT PAN ANGLE ******	0.1	10	01	01	70	01	01	70	10	10	70	10	10	10	10	07	01	01	01	01	10	10	10	10	01	01	07	07	07	20	20	20	20	20	70
BACK REST ANGLE ******	~	1 11	13	13	13	13	13	27	27	27	27	27	27	27	51	51	51	51	51	51	51	65	65	65	65	65	65	65	65	65	65	65	65	65	9

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Upper Torso Information Head Position 1

		·		
>	12.26	1.61	125.10	. 6 ° L
۸Ι	12.63	1.83	124.20	1.77
111	13.33	1.03	112.00	2.39
II	12.75	0.63	97.10	4.80
I DS	11.87	0.76	90.30	3.30
	e Wean	Upper Back Distanc		Helme Angl Std, Dev.
		Joeg woudth	0+ weod +	~~ [~ H

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UPPER TORSO INFORMATION Head Position 2

-				
۸	12.43	1.73	119.90	7.52
١١٧	12.52	1.74	121.00	4.61
III	12.41	1.64	107.50	4.89
11	12.53	1.34	79.40	7.30
SC I	12.58	1.14	68.90	7.26
	Меал	Std. Dev.	Wean	Std. Dev.
	ə:	Distanc	1	ГриА
		Nbber Back	ot nean to	нејше

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UPPER TORSO INFORMATION Head Position 3

>	13.47	1.44	126.70	2.16
۱V	13.88	1.45	126.60	2.23
111	13.74	0.88	113.70	2.20
II	11.41	1.01	113.60	5.57
SC I	11.45	0.83	102.70	4.99
	Mean	Std. Dev.	Меал	Std, Dev.
	90	Distan	et Rear to	buA

UPPER TORSO INFORMATION Head Position 4

		3		
>	12.35	1.52	124.00	5.74
١٧	12.57	1.61	124.40	2.61
III	12.08	1.30	111.60	2.30
II	10.64	1.15	97.70	8.53
SC I	10.12	0.99	89.30	6.93
	Mean	Std. Dev.	Mean	Std. Dev.
	9;	Upper Back Distanc		en ren EgnA

UPPER TORSO INFORMATION Head Position 5

۸	12.00	1.74	124.40	4.80						
IV	12.12	1.46	124.80	2.97						
111	11.63	1.35	111.50	3.13						
11	10.21	1.01	100.00	8.97						
SC I	9.78	1.21	89.20	8.30						
	Меап	Std. Dev.	Mean	Std. Dev.						
	t	nstrid		Би ү						
	Helmet Rear to Upper Back									

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UPPER TORSO INFORMATION Head Position 6

۸	12.10	1.79	123.70	3.04
۸Ι	12.77	1.65	125.10	2.90
111	11.98	1.64	111.10	2.50
11	10.84	1.31	103.50	8.64
SC I	10.34	1.14	94.30	& *: &
	Mean	Std. Dev.	Mean	Std. Dev.
	ə:	Distanc	ð	ſpnA
		Npper Back	t Rear to	Helme

APPENDIX A-2
Menton Data

HEAD POSITION 1 BACK REST ANGLE IS 13 SEAT PAN ANGLE IS 10

NALE Y DEL-2 *******	-4.33	-3.74	L 2	Ç.	5	4.0	_	-4.75	3.5	พ้	3	4.1	-	0	-3.86	0		-3.52	rr.	0	0.38
STERNA DEL-Y *****	0.04	-0.04	N	-	0.0	-	S	-	0	Š	-0.53	-0.24			+0.0-	~	\sim	80.0	3	0.10	6
0 SUPR DEL-X *****	-0-99	-1-85		ċ	$\ddot{-}$	-	•	2	2	ä	•	(4	~	•	4	-		4	•	•	0.57
4ENTON T DISTANCE *********	4. 442 4. 805		07	37	93	3.4	57	27	2 8	95	C	-4	6	2	5	-	-	3.973	~	S	0.49
TO UPPER BACK ANGLE *******	91.4 95.6	90.2		\$	6	\$	å	•	9	4	+	-	ŝ	7	٠ م	0		ċ	•	•	3.30
HELMET REAR TI DISTANCE *******	11.574	11.288	6	8.0	2.7	2.6	2.1	2.1	1.9	2.5	2.3	1.6	0.0	2.7	1.5	1.3	8.4	-	3.4	11.875	92.0
SUBJECT	ጣሪጣታዩ	101	· œ	0	70	77	12	13	14	15	16	11	18	19	20	21	22	23	24	Z	STD DEV

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Annual Company of the Company of the

65.0 -4.67 -3.50 -3.73 -3.22 -4.02 -3.43 -4.00 3.57 -3.31 -3.24 -3.91 -3.35 -3.15 -3.37 64.4--3.07 -4.11 -2.87 2-13Q MENTON TO SUPRASTERNALE ANCE DEL-X DEL-Y DE 0.12 0.037 -0.28 -0.09 0.54 0.00 0.00 0.42 0.17 -0.17 -0.29 0.04 0.12 -0.08 -0.39 0.0 -1.24 0.71 -i-88 -0.53 -1.84 -1.04 -1.22 -2.17 -1.80 -1.39 -0.61 0.70 -2.05 -1.14 -1.48 -1.52 -0.62 -0.53 -1.80 11.1--0.28 3.846 DISTANCE 4.321 3.874 4.239 3.663 3.718 3.659 5.006 3.973 3.786 3.827 3.202 3.409 3.240 3.382 4.569 4.6.57 3.229 2.957 3.464 SI SEAT PAN ANGLE UPPER BACK ANGLE 4.80 98.3 98.3 98.5 100.5 92.6 95.3 91.3 92.0 94.8 90.8 95.9 97.1 10001 96.8 *** 001 10 HELMET REAR DISTANCE 27 12.746 12.748 12.888 13.208 11.836 13.103 11.761 13.023 12.761 11.278 12.649 13,238 12.447 13.770 2.294 3-395 SI REST ANGLE PUSITION 1 STD DEV MEAN VL SUBJECT 11 15 11 15 11 11 222 222 223 233 233 HE AD BACK

AND AND AND ASSESSED AND ASSESSED ASSES

HEAD POSITION 1 BACK REST ANGLE IS 51 SEAT PAN ANGLE IS 10

SUBJECT	HELMET REAR TO DISTANCE *******	UPPER BACK ANGLE ******	MENTON DISTANCE *******	10 *	SJPRASTERNA =L-X DEL-Y ********	ALE DEL-Z ******
~ N M 4 1	14.385	112.4	2.347	-0.28	0.04	-2.33
n o r	3.38	14.	.99	S	0.08	0.4
∞ •	3.41	10.	.16	6.	N 00	241
	2.70	12.	50.	2.6	. ~	2.5
	1.19	10.	46		0 4	4 -
4 4 6	13.058	110.6	2.918	-0.62	0.25	. 2 2
	3.03	12.	10	, m,	9	2.7
	4.26 1.34	15.	.51 .49	. C.	o m	٠. 4
	2.94	11.	•39	7-	-0.30	3.3
	2.44	• † • † • † • † • † • † • † • † • † • †	.84	: -:	φ,	2.7
	2.72	12.	.62		0.30	2.4
	3.04	12.	•43 •16	-0.73	0.0	ي ا
MEAN VL STD DEV	13.327 1.03	112.0	2.828 0.64	-0.24	0.14	-2.76 0.66

HEAD POSITION 1 BACK REST ANGLE IS 65 SEAT PAN ANGLE IS 10

ALE DEL-Z ******	-1.99	1.3	4 4 6 4	-2.60 -2.27 -2.84 -3.23	22.0	-2.27 0.61
STERN DEL-Y ****	0.26	40.4.	0.00	0-1001	0.00	0.07
TO SUPR DEL-X :*****	0.34 0.08	ムカント	M M O & .	0.24 0.35 0.35 0.35 0.37	シーシーチ	0.25
MENTON DISTANCE	2.036	25 22 22	2222	2.612 2.271 2.296 2.859 3.251 3.176	89223	2.357 0.59
10 UPPER BACK ANGLE	122.2	24.23.	24. 24. 23.	121.9 124.8 124.3 125.3 125.3	25.25.25.24.24.24.	124.2
HELMET REAR T DISTANCE *******	13.279	46.94 4.54 20.32	4.56 4.56 4.56 4.86	11.382 15.267 14.046 14.375 10.376	9.92 9.60 0.90 0.96 1.72	12.632
SUBJECT	→ 01 m 4 m	1 0 ~ 0 0		11 12 14 15 14 15 14 15 15 15 15 15 15 15 15 15 15 15 15 15		MEAN VL STD DEV

-2.35 -3.24 -1.96 -2.30 -2.03 -2.26 -1.97 -0.89 -1.85 -2.10 -1.40 MENTON TO SJPRASTERNALE
DISTANCE DEL-X DEL-Y DEL-Z -1.77 -2.69 -2.80 -1.42 -2.65 -0.12 0.34 -0.17 0.0 0.51 -0.08 0.05 0.00 0.00 0.00 0.00 0.02 0.03 0.03 0.13 -0.16 0.37 0.46 0.90 0.54 0-77 0.24 94.0-0.61 0.33 -0.41 0.47 0.62 0.02 80.0-2.671 2.695 3.261 3.366 1.531 1.502 1.951 2.429 2.170 2.941 2.033 2.418 2.140 2.105 2.556 2.335 2.047 1.062 15 SEAT PAN ANGLE HELMET REAR TO UPPER BACK DISTANCE ANGLE 1.53 123.8 123.8 123.6 125.8 126.8 127.5 129.0 126.5 124.2 PARTHER ANGLE 125.2 126.5 125.4 123.1 128.0 123.2 123.1 123.8 122.1 124.1 126.9 HEAD POSITION 1 BACK REST ANGLE IS 65 11.982 12.586 13.054 12.353 12.184 13.769 14.654 11.322 10.728 11.134 8.386 10.885 10.338 13.640 14.297 14.306 13.685 12.261 1.61 SUBJECT MEAN VL STD DEV

A the state of the same of the state of the

-1.07 -1.81 1.43 -0.34 -1.81 -1.72 -0.63 -2.66 -2.20 -3.18 -1.11 -1.73 -0.78 -1.93 -0.12 -0.34 -0.66 MENTON TO SJPRASTERNALE DISTANCE DEL-X DEL-Z 0.02 -0.20 0.0 -0.08 0.53 -0.25 0.00 -0.52 0.12 0.45 0.21 0.0 0.0 0.01 -0.94 -1.40 -1.40 -1.47 -0.74 -0.17 -1-18 -0.10 -0.7× -0.0 B -0.78 -0-13 -0.78 -1.52 -1.59 -0.66 +5.1-1.782 2.288 1.946 0.781 2.761 2.638 1.034 3.503 2.444 1.917 1.653 2.276 0.376 1.327 0.144 0.664 0.851 2 21 SEAT PAN ANGLE HELMET REAR TO UPPER BACK DISTANCE ANGLE 68.9 80.3 61.0 61.2 77.0 70.9 64.4 65.1 73.3 71.2 75.8 75.1 72.6 63.8 75.1 58.9 PUSITION 2 REST ANGLE IS 13 12.585 13.601 12.367 11.641 11.840 11.685 12.623 12.060 13.489 13.365 12.013 11.786 11.730 13.080 15.623 13.057 MEAN VL STD DEV SUBJECT HEAD

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-0.36 -1.86 -0.31 -2.29 -1.35 0.71 DEL-Y DEL-Z -0.96 -1.19 -1.97 -1.30 -2.35 -1.44 -2.36 -2.70 -0.80 -0.67 开关 法托托法 经资本 天安天 安安安 安安 医牙牙 多子 医子子氏病 医多种 -1.46 -0.77 -1.62 -0.36 -1.21 MENTON TO SJPRASTERNALE 0.04 0.05 +0.0-0 0.45 0.11 0.0 0.54 0.12 0.46 -0.04 0.08 0.21 -0.04 -0-12 0.0 0.0 DEL-X -0.08 -0.70 -1.40 -1.50 -0.37 -1.64 -0.82 -0.90 79.0--0.58 0.61 -1.43 0.55 0.04 -0.90 -0.36 -1.43 -0.61 -0.08 -0.20 -0.82 DISTANCE 0.369 1.036 2.876 2.418 1.304 1.753 1.772 2.433 0.845 1.197 2.391 1.871 1.357 1.638 1.579 0.766 0.796 SI SEAT PAN ANGLE HELMET REAR TO UPPER BACK DISTANCE ANGLE 79.4 71.0 83.5 64.5 82.4 83.1 83.4 84.5 84.3 64.4 84.8 78.9 80.7 71.0 79.1 *** 27 12.651 10.963 12.467 11.853 16.539 12.434 14.657 11.763 11.443 14.273 12.022 12.339 10.372 12.343 12.534 11.853 12.829 12.359 12.535 REST ANGLE IS 12.381 1.34 POSITION 2 MEAN VL STD DEV SUBJECT HEAD BACK 20 21 22 22 23 24

	DEL-Z *****	-1.13 -1.78	-1.75	9	.	4	7	•	7.	œ	2.1	S	7	2.3		•2	5	۲.	• 9	4.	8	-1.67	4.
	AST ERNA! DEL-Y ******	0.34	0	0.04	٠	0	0	-4	0.38	-0-17	•2	7	0	0.0	0.0	0.0	0.0	~	0.12		-0.08	0.03	~
	TO SJPR DEL-X	-0.03	-0.58	97.0	S	•	3	4.	.2	•		4.	4	6	7	•	?	λ.	-0.20	3.	0.30	•	C.46
15 10	MENTON DISTANCE #******	1.180 1.798	•	1.709	649	04.	•29	.15	. 18	.88	•15	000	.61	.35	.30	.30	.52	16.	.93	.51	.88	.7	0.47
SEAT PAN ANGLE	AR TO UPPER BACK CE ANGLE #********	105.1	O	ئ	C 8 •	03.	10.	04.	•66	12.	CB.	13.	00	12.	10.	1,	11.	98.	8	.90	2.	107.5	•
TION 2 ANGLE IS 51	HELMET REAR ' DISTANCE ************************************	12,463	3.80	13.890	2.76	1.85	2.39	4.48	0.11	60.4	3.03	3.55	3.51	4-82	8.61	.51	74.6	2.32	.58	2.90	1.65	12.406	1.64
HEAD PUSI BACK REST	SUBJECT	። ሀ ፡፡፡ 4 ፡፡	9	1	80	6	10	11	12	13	14	15	91	17	1.8	19	20	21	22	23	24	N	STO DEV

-1.75 -1.36 -1.41 MENTON TO SUPRASTERNALE DISTANCE DEL-X DEL-Y DEL-Z 0.0 0.0 0.0 0.22 0.25 0.25 -0.21 90.0 -0.26 0.08 -0.21 0.04 0.39 0.04 -0.05 0.21 -0-13 60.0-0.62 0.33 0.25 0.36 0.58 0.54 **+1.0-**-0.36 0.60 1.440 0.920 1.363 1.612 1.178 1.314 1.479 1.200 2.688 1.085 1.928 1.965 1.540 1.117 1.578 2.254 1.543 1.299 SI SEAT PAN ANGLE UPPER BACK ANGLE 122.3 121.5 112.6 126.2 24.8 125,6 127.5 121.6 122.4 123.0 6.111 125.1 113.6 ************* 10 MET REAR DISTANCE 65 14.969 13.547 10.415 11.901 11.456 14.324 10.827 14.337 12.440 13.060 13.214 12.264 14.106 9.209 14.857 12.714 14.411 9.787 POSITION 2 REST ANGLE IS HELMET SUBJECT HEAD BACK 20 22 23 24 24

-2.47 -1.82 -1.38

-1.12

-1.18

-1.16

-1.34

-0.98

-0.74

-1.90

-2.24 -1.92

-1.02

-1.43

96.0-

-1.39

-1.35

-1.45

-0.01

0.19

1.555

19.5

121.0

12.523

MEAN VL STD DEV

0.43

HEAD POSITION 2 BACK REST ANGLE IS 65 SEAT PAN ANGLE IS 20

1ALE ' DEL-Z :*****	-1.15	1.6 1.0 0.9	-0.87 -1.16 -0.93		-2.18 -2.18 -2.01 -2.05 -0.94 -1.27	-1.41 -1.41 0.45
SJPRASTERNALE EL-X DEL-Y D *********	0.34	-0.39 0.26 -0.17	46.0- 0.0 0.09	0.85	0.00	0.03
	-0.16	0.75	0.82	0.81 0.49 0.849	0.45 0.45 0.75 0.73 0.73 0.73 0.73	0.24
MENTON DISTANCE	1.210	70 32 33	28 42 26 26	0 4 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	1.556 2.226 2.073 2.176 1.060 1.611	1.571 1.610 0.42
O UPPER BACK ANGLE *******	115.7	86.9	4500	4042	124.5 124.5 127.0 104.5 112.3	125.2 119.9 7.52
HELMET REAR T. DISTANCE *******	11.445	81	224	2	13.800 15.009 12.144 13.304 11.052 12.654 11.553	10.8C1 12.427 1.73
SUBJECT	⊶ <i>∕</i> 1 w 4`n	o → o ∕	100	11111 1241 134	16 17 18 20 21 22	23 24 MEAN VL STD DEV

HEAD POSITION 3 BACK REST ANGLE IS 13 SEAT PAN ANGLE IS 10

SUBJECT	HELMET REAR TO DISTANCE *******	UPPER BACK ANGLE	MENTON DISTANCE	TO SUPR DEL-X ******	SUPRASTERNAL :L-X DEL-Y :*******	LE DEL-2 *****
ግ ረ መ ላ ል	12.214 10.959	102.4	7.121 9.303	-1.72	0.04	-6.91
19 ~	.48	99.	.29	8.7		00
& 6	1.57	00	92	1 - 1	9.7	8 8
	3.18	92.	.22	2.6	3	7
	1.59	4 4	.32	0.7	7 9	7.2
1 1 1 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	11.6252 10.872 12.361	7000	6.426 7.499	-2.10	0.20	-6-07
	1.21	2.	91	2.1	0.6	6.5
	0.90	01.	· 9 N	1. g	m 0	7.4
	0.07	-0	95	34	2.4	7.0
	0.84	0.8	65	1.9	00	4.4
	36	07.	11	.	•2	-6.98
MEAN VL STD DEV	11.450	102.7	7.092 0.73	-1.72	0.22	-6.83 0.78

HEAD POSITION 3 BACK REST ANGLE IS 27 SEAT PAN ANGLE IS 10

SUBJECT	HELMET REAR TO DISTANCE ********	D UPPER BACK ANGLE *******	MENTON DISTANCE *******	TO SUPRI	ASTERNA DEL-Y *****	LE . DEL-2 *****
	12.180	113.3	7.294 8.840	-0.21	0.13	-7.29 -8.76
, o ~ a	0.57	4.6.5	28	0.20	0 ~ 4	6.1
9 6 0	1.50	15.08	63		0.50	6.6
117	2.95	C8.	55 12	0.90	0.17	6.4 7.1
13 15 15	63 20 71	18. 95. 13.	97 29 54	-0.32 -2.67 0.0	007	6.9 5.7 7.5
16 17 18	1.44 1.44 9.85	13.	527	-1.56 -1.15 -0.69		6.3 6.6 5.3
19 20	72	13.	02	06.0-	0.7	6.9 7.1
21 22 24 24	12.154 10.858 11.486 11.083	111.1 121.5 112.5 123.1	7.299 7.235 6.780 7.322	-0.78 -0.16 -1.19 0.41	0.20	-7.20 -7.23 -6.66 -7.31
MEAN VL STD DEV	11.409	113.6	6.815 0.77	-0.50	0.25	-6.73 0.81

HEAD POSITION 3 BACK REST ANGLE IS 51 SEAT PAN ANGLE IS 10

SUBJECT ======	HELMET REAR TO DISTANCE ************************************	O UPPER BACK ANGLE *******	MENTON DI STANCE *******	TO SUPRAS DEL-X C	TERN)EL-V	IALE ' DEL-Z :******	
→ N M 4 1	14.232	115.6	5.910	0.10	0.21	-5.85	
n o r	3.80 1.96	11	~ 0	ဘာထာ	0.13	-4.64	
დ თ	13.596	114.4	16	-0.45	0.04	-4-14	
10	2.82	13.	<u>~</u>	00 4	0.25	4	
77	3.99	11.		9 1		י מו כ	
14	3.30 4.38	12.	000	91.	0.17	0 4	
15 16	4.172.70	14.	93	5 3 6 4		-5.91	
17	3.30	15.	11	2016	0 -	S	
19	3.65	16.	20	3	-0.50	7	
20	3.37	16.	9.	00		-6.49	
22	4.35	14.	. 6	, w	m	·N	
23	2.39	13.	24	9	0.33	41	
54	4.4	70.	6	0.1	.2	-5.88	
MEAN VL STD DEV	13.741	113.7	5.823 0.98	-0.81 0.68	0.13	-5.71	

HEAD POSITION 3

	LE DEL-2 *****	-6.47	.2	3	3.2	. a	4.0	0	, ,	-4.78	6.3	4.7	7	α,	6.1	5.4	1	7.	0	5.2	-5.28	٦.
	STERNA DEL-Y *****	0.12	•2	7	40.0	,	0.0 40.0	ڻ ر	7-	-0-21	0	3	J	0.16	8	0.0	0	0.72	4.	•	0.04	4.
	TO SUPRA DEL-X ******	1.07	0.0	0.00	~	m.	┥、	د ه	ب ر	7.70	7	1	0	Ø	7	0	0	•	-1.22	0.08	0.42	70
15 10	MENTON DISTANCE *******	6.559 6.843	24	37	25	82	ָ קיי	2 0) (4.791	50	81	71	0	81	45	15	18	26	77	5.373	• 2
SEAT PAN ANGLE	G UPPER BACK ANGLE *******	130.7	•	- 1	<u>.</u>	.	•		•	126.3		•	•	ch Ch	ů	•	7	5	•	8	•	2.23
IUN 3 ANGLE IS 65	HELPET REAR T DISTANCE *******	15.679	4.47	3.88	3.05	E2.8	3.95	3.44	0 · · · · · · · · · · · · · · · · · · ·	15.579	5.18	4.08	3.88	2.85	2.21	0.84	5.70	3.75	1.00	3.07		4.
HEAD FUSION BACK REST	SUBJECT		۰.0	7	©					15											Z	STD DEV

HEAD POSITION 3 BACK REST ANGLE IS 65 SEAT PAN ANGLE IS 20

SUBJECT	HELMET REAR TI DISTANCE	O UPPER BACK ANGLE *******	MENTON DISTANCE *******	TO SJPR DEL-X ******	SJPRASTERNA EL-X DEL-Y *********	LE DEL-Z *****
= 06	15.116	128.7 124.3	6.132 7.589	0.87	0.60	-6.04 -7.31
400-	1.15	9 9	99	2.7	-0.12	13.99
· 00 (D*	2.42	S S	59	~ ^	-0.51	-4.55
	13.596	126.0	69 17	A .	-0.04	-3.69
	3.63	4.8	64 40	A1 A	0.60	-4.60 -6.21
40.4	4.95	27.	6.515 5.860 4.853	0.33	0.17	-4.50 -5.81
	14.153	124.3	9 9 9		0.04	-3.93
	4.32	29.	73	~ ~	-0.34	-6.68 -6.13
	3.88	30.	6 5 0 6		0.72	-7.23 -5.02
	3.25	25.	87	m a	0.89	-4.71 -5.47
MEAN VL STD DEV	13.466	126.7	5.423	0.40	0.09	-5.32 1.10

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HEAD POSITION 4 BACK REST ANGLE IS 13 SEAT PAN ANGLE IS 10

ALE ' DEL-Z :*****	-3.47	490	1000	14mmmm	20806	45 44
ASTERN DE:L-Y	3.77	6.4	6.1.9	3 8 4 7 0 8 4 7 1 0 0 8 4 7 1 0 0 8 8 7 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	4.4.8.	1. 2.
TO SUPR DEL-X *******	0.45	400	0.27 0.12 0.04 0.24	0.34 0.34 1.13 -0.08	1.97 -0.45 2.95 0.66	-0.03 -0.82 0.38
MENTON DISTANCE	5.144	56 9 3 9 3 9 9	577	5.981 6.085 5.003 5.042	50 40 80 80	Q 0 04
O UPPER BACK ANGLE *******	77.5 92.7	7.7	51744	0 -1 0 %	106.9 85.6 109.6 90.7	0 m 0 0
HELMET REAR TO DISTANCE	11.073	1.86 9.45 0.65	23 20 20 20 20 20 20 20 20 20 20 20 20 20	9.7	7.811 11.463 8.344 10.131 9.440	9.741 10.958 10.119 0.99
SUBJECT	N M 4 K	1010		124 13		

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-3.13 -3.02 -3.00 -2.58 -3.07 -2.85 -3.72 -3.76 -2.96 -3.56 -4.47 -3.28 -2.91 -3.09 -2.91 -3.25 -2.96 -2.69 -3.03 DEL-X DEL-Y DEL-Z -2.61 MENTON TO SUPRASTERNALE 3.38 3.47 3.80 3.84 4.35 4.34 4.51 4.13 3.30 3.98 3.40 4.17 4.38 3.38 66.4 4.39 3.32 0.56 1.89 0.10 -0·18 -0.45 1.68 1.05 0.64 1.58 3.39 1.34 1.19 1.12 0.67 0.77 DISTANCE 4.287 6.858 4.900 5.237 4.597 4.905 5.453 5.404 5.491 6.271 5.370 5.335 6.404 6.045 4.663 5.229 4.661 6.405 5.508 5.094 SI SEAT PAN ANGLE HELMET REAR TO UPPER BACK DISTANCE ANGLE 8.53 55.8 107.7 99.9 91.3 98.5 97.4 94.3 81.8 95.1 123.3 91.2 93.9 92.1 90.4 21.1 102.8 94.1 **** 101.4 9.901 104.3 HEAD POSITION 4 BACK REST ANGLE IS 27 11.473 10.520 12.002 9.617 11.456 10.642 11.920 11.084 li.166 9.764 10.363 11.967 9.767 9.753 10.778 9.953 6.953 0.945 0.457 11.831 MEAN VL STD DEV SUBJECT 222209844 222209846 232209846 2432109846

-2.19 0.71

3.90

1.69 0.68

4.844 0.82

1111.6

12.078 1.30

MEAN VL STD DEV

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-1.07

-2.41

-2.58 3.93

-1.79 -2.49

-1.8

-2.18 -2.17 -2.39 -1.93 -1.93 -1.23 -1.22 -1.78

-2.07

MENTON TO SUPRASTERNALE DISTANCE DEL-X DEL-Y DEL-Z 3.08 .65 .26 .85 1.48 1.61 4.314 4.108 4.108 4.431 3.971 4.219 4.129 4.492 4.244 6.196 5.740 5.587 4.578 4.694 4.601 IS SEAT PAN ANGLE HELMET REAR TO UPPER BACK
DISTANCE ANGLE 110.5 110.0 111.9 112.9 114.8 109.7 107.1 110.2 109.7 106.9 113.3 114.7 112.4 114.6 112.0 51 10.815 12.067 11.947 12.190 12.298 12.772 11.647 12.302 10.137 12.202 12.071 11.764 10.902 13.996 14.273 12.702 15 POSITION 4 REST ANGLE SUBJECT 11 (1 11 11 11 HEAD B

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HEAD POSITION 4 BACK REST ANGLE IS 65 SEAT PAN ANGLE IS 10

LE DEL-2 *****	-1.01	1.8	72.00	4.6.7.	-2.21 -2.82 -1.12 -1.99 -1.39 -2.3¢	-1.74
PRAST ERNA: X DEL-Y: ************************************	3.29	0971	1426	4.31 3.28 2.90 3.84	4.70 4.78 4.09 3.16 2.70	3.64
TO SU DEL- ****	3.27	~ · · · ·	36.46	3 4 4 4	2.72 3.54 3.54 1.73 1.74	2.13
MENTON DISTANCE ********	3.762 5.633	.94 .60 .21	67 67 74		5.863 6.372 5.765 3.438 3.675	4.001 0.85
O UPPER BACK ANGLE	124.0	23.	26. 24. 24.	2222	126.3 126.2 126.2 127.2 123.5 124.6	124.4 2.61
HELMET REAR TO DISTANCE	13.768	4.78 2.55 2.15	2 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	80 84 74 50 13	10.252 12.335 9.861 11.562 10.464 12.465	12.571
SUBJECT	N 60 4 1	n	10 11 12	113 15 16 16	118 20 22 23 24	MEAN VL STD DEV

HEAD POSITION 4 BACK REST ANGLE IS 65 SEAT PAN ANGLE IS 20

SUBJECT	HELMET REAR TO CISTANCE *********	UPPER BACK ANGLE	MENTON DISTANCE *******	TO SJPR, OEL-X *******	AST ERNA DE L-Y ******	LE DEL-2 *****
⊣ 0m45	12.657	122.7	3.886 6.515	1.78 3.68	3.42	-0.49
n	1.07	20.	.26	0 2	6.	٠. دي -
- co (11.042	126.9	1 M 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	1.65	2.56	4 (
	2.66	27.	11.	• -:	. w	
11	1.91	01.	37	8 ~	0,0	. 2
	5.75	26.	.87	7	7	8
	4.69	22.	.20	7.	5.	٠. ش
	2.25	25.	.88	?	3	. 7
	3.00	28.	.56	6.	4.	2.3
	5 5 • 1	25.	.85	8	6	4.
	4.02	27.	. 58	•	1.	•2
	1.38	28.	.82	3	0	ŝ
	2.05	27.	9	6•		• 6
	649	23.	. 43	9	80	1.0
	11.345	127.6	3.694	79.1	2.53	-2.15
MEAN VL STD DEV	12.348	124.0	4.484 0.91	2-11	3.53	-1.59

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-1.58 0.61 -1.58 -2.90 -2.13 -1.84 -1.32 -1.90 -2.42 -2.03 -2.20 -2.56 -0.56 -1.44 -1.98 -2.00 -1.05 -2.48 -1.55 -0.58 -2.33 DEL-Z MENTON TO SUPRASTERNALE 3.67 2.93 3.71 3.72 3.22 3.56 4.48 4.15 3.96 3.37 4.92 3.22 4.04 2.73 3.50 3.16 DEL-X DEL-Y 0.76 -0.27 0.50 -0.02 1.76 2.44 0.06 1.84 2.35 -0.03 1.04 0.00 1.12 0.35 0.75 0.20 1.27 -0.18 DISTANCE 4.227 4.503 3.884 3.505 4.607 3.387 3.916 3.594 3.915 5.890 4.434 4.230 3,430 4.459 5.606 4.662 4.131 4.314 99.0 SI SEAT PAN ANGLE HELMET REAR TO UPPER BACK DISTANCE ANGLE 89.2 8.30 6.56 90.6 55.6 88.9 87.0 88.3 54.1 77.8 81.0 85.9 86.7 86.5 100.3 112.3 74.8 88.2 15 13 9.776 10.760 9.801 9.144 10.312 10.795 8.140 9.756 7.594 10.180 10.581 10.098 10.134 9.033 0.623 8.425 9.315 11.554 11.017 POSITION 5 REST ANGLE STD DEV MEAN VL SUBJECT 11 11 11 11 11 HEAD 450180

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HEAD POSITION 5 BACK REST ANGLE IS 27 SEAT PAN ANGLE IS 10

SUPRASTERNALE :L-X DEL-Y DEL-Z :*********	3.10 -1.17 4.57 -1.28	2.98 -1.5 3.49 -0.6 2.72 -2.1 4.07 -1.2 3.94 -1.9 5.72 -1.6	3.22 -2.94 3.73 -1.98 3.61 -1.29 2.81 -1.28 4.19 -1.55 5.16 -1.85 3.93 -2.09 4.25 -3.19 4.08 -2.46 4.18 -1.39 3.19 -2.74	3.77 -1.75 0.61 0.67
0 + 30 * * *	0.93 2.19	000000	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	1.57
MENTON DISTANCE	3.441 5.227	9 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 -	4.391 4.316 4.316 6.071 6.198 7.27 7.27 7.865 7.016	4.486 0.79
TO UPPER BACK ANGLE *******	95.1	00000	966.5 103.2 103.2 103.2 103.2 113.2 6.7.4 9.4.4	100.0
HELMET REAR DISTANCE	11.103	9.34 9.34 9.75 9.99 9.88	10.478 10.232 9.943 10.076 11.038 8.238 11.269 8.440 10.231 8.623 9.186	10.214
SUBJECT	⊶ U M 4 W	8 4 7 8 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	11 11 12 12 13 14 14 17 17 17 17 17 17 17 17 17 17 17 17 17	MEAN VL STD DEV

-1.08 -0.43 -0.85 -0.86 -1.53 -0.71 -1.10 -1.01 DEL-Y DEL-Z -0.59 -1.13 -0.85 -1.01 -0.03 -1.46 -0.46 -1.04 -1.44 -0.01 -0.07 -1.46 -0.81 MENTON TO SUPRASTERNALE 2.70 3.28 3.28 3.28 3.29 3.21 2.91 3.09 3.46 4.46 3.20 3.43 3.72 3.84 2.84 DEL-X 1.81 1.51 1.32 1.54 69.0 1.44 1.16 1.80 1.03 1.43 2.12 2.16 1.85 1.61 0.46 1.57 DISTANCE 4.03.65 4.03.65 4.03.65 4.03.65 4.03.65 4.03.86 4.0 3.723 3.347 3.722 4.536 4.213 3.915 3.422 4.338 SI SEAT PAN ANGLE HELMET REAR TO UPPER BACK DISTANCE 3.13 112.6 110.6 112.3 108.1 1111.0 113.0 1111.0 114.8 103.4 113.8 112.7 114.6 114.2 110.4 111.9 116.0 25 12.803 11.632 12.658 11.162 12.210 9.582 14.473 11.634 12.429 8.708 10.144 11.650 11.982 12.353 10,643 10.458 10.230 HEAD POSITION 5 BACK REST ANGLE IS MEAN VL STD DEV SUBJECT 11 11 11 11 11 11 11

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0.48 -0.51 0.44 -0.43 -0.87 -0.09 -0.56 0.02 -1.10 -0.43 -0.54 -1.02 -0.55 -0.80 -0.65 0.07 -0.50 -0.07 -0.81 DEL-Y DEL-Z MENTON TO SJPRASTERNALE DISTANCE DEL-X DEL-Y DE 44. 3.49 3.46 3.24 4.31 3.88 3.58 3.11 2.86 3.02 3.02 3.28 3.28 3.38 3.38 3.38 3.15 3.46 3.81 3.27 2.57 2.28 2.10 1.70 2.46 2.07 0.40 1.90 2.34 2.05 2.44 1.40 2.63 3.05 1.60 1.38 2.11 2.48 4.083 4.174 4.020 3.616 4.100 3.603 4.963 5.070 4.627 3.126 4.486 4.313 4.178 3.942 4.195 3.717 3.734 3.324 4.431 2 SI SEAT PAN ANGLE UPPER BACK ANGLE 2.97 124.4 128.2 127.3 127.2 124.8 124.4 122.2 133.1 123.1 125.0 127.8 119.9 123.6 122.3 124.7 122.7 125.2 121.3 120.9 *** 10 HELMET REAR DISTANCE BACK REST ANGLE IS 65 10.352 12.118 .450 13.131 11.910 12.364 12.450 14.803 11.483 10.508 11.863 10.132 10.664 11.632 14.168 11.809 13.327 13.854 11.094 15.171 1.46 HEAD POSITION MEAN VL STD DEV SUBJECT 20 22 22 23 24 61 18

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ALE DEL-2 ******	-5.90	-4.34	-4.76	-5.30	-6.16	-6.78	-6.36	-5.61	-4.70	-6.48	-6.27	-7.39	-6.55	-4.28	-5.70	-5.72	0.92
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-5.38 -4.43 -4.51 -6.62 -5.30 -5.18 -6.40 -5.09 -4.10 DEL-Y DEL-Z -5.13 -4.75 -4.30 -5.24 -4.54 -5.83 -5.62 -5.82 -6.06 计计算符件 计计算计 法计算法 计计算法 计计算计算 计计算机 计计算机 -6.61 MENTON TO SUPRASTERNALE 1.65 4.50 3.84 69.4 3.56 3.75 2.88 3.09 3.50 3.30 3.04 3.25 3.28 3.10 4.14 2.92 3.01 DEL-X 0.91 3.59 0.58 2.73 0.39 3.37 2.50 2.15 2.05 0.26 1.88 -0.23 1.31 1.05 24.0 0.80 -0.03 2.90 10.0 -0-14 DISTANCE 5.700 5.575 6.389 5.948 6.711 7.056 7.305 6.939 7.921 7.202 5.275 6.431 5.736 5.991 6.708 6.519 6.031 6.360 0.78 15 10 SEAT PAN ANGLE HELMET REAR TO UPPER BACK 8.64 98.3 117.7 100.5 98.3 109.6 96.2 102.9 7.18 96.6 100.4 DISTANCE ANGLE 101.2 97.3 85.4 103.5 109.8 113.6 REST ANGLE IS 27 11.493 12.288 9.937 11.303 9.299 11.465 13.148 11.155 10.020 12.300 8.559 11.953 10.605 10.837 11.369 11.561 10.153 11.581 9.781 10.852 1:31 PUSITION 6 MEAN VL STD DEV SUBJECT 11 11 11 11 11 11 HEAD BACK 19

HEAD POSITION 6 BACK REST ANGLE IS 51 SEAT PAN ANGLE IS 10

ERNALE :L-Y JEL-Z :*****	.43 -4.64 .28 -5.26	21.	98 -3 6	.60 -3.6 .95 -4.6	15 -4.7	08 -3-4	15 -4-7	7·5· 55·	.01 -3.9	.33 - 6.2	2.4 62.	76.	2-4- 16-	.74 -3.	0.	.04 -4.56
TO SUPRAST DEL-X DE *********	3.95 4.	.93 .35 .2	20 20 20 20 30 30 30 30 30 30 30 30 30 30 30 30 30	09 3 14 2	23 2 2	12.	72 2	12 3	.20 4	.43 .43		010	. d8.	53	0 97.	1.51 3
MENTON DISTANCE *******	5.073	5.305 5.504	72	N N	97	~ ~	9 /	ת כ	0	2	8	2	5	36	8	5.872
O UPPER BACK ANGLE *******	114.1		108.5	10.	150	13.		12. 09.	60		77	14.	12.	5	115.6	1111.1
HELMET REAR T DISTANCE *******	13.152 13.618	92	12.368	22.2	0.42	4.52	1.73	1.49	0.87	,))	.10	3.72	1.96	0.30	14.040	11.981
SUBJECT	H 01 M 4	· w o r	- თ თ	10	12	13	15	16	- F	16	20	2.1	22	, c	24	MEAN VL

HEAD PUSITION 6 BACK REST ANGLE IS 65 SEAT PAN ANGLE IS 10

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517 131.5 5.191 855 124.4 4.478 361 124.7 4.395 287 127.7 4.395 421 120.0 6.900 978 126.5 6.900 189 126.5 6.900 189 122.1 5.209 102 121.2 5.209 102 121.2 5.209 103 121.2 5.213 104 125.0 6.994 715 125.0 6.994 715 125.0 6.994 715 125.0 6.585 850 127.2 6.585 850 126.4 4.716 223 129.3 6.223	127.	68	5	.2	.2
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UPPER TORSO INFORMATION
Head Position 1

			3C I	II):II	IV	v
	çe Çe	Mean	4,52	3.846	2,83	2.36	2.33
	Distance	Std. Dev.	0.49	0,54	0.64	0.59	0.65
o)	e X	Mean	-1.83	-1.24	-0.24	0.25	0.24
Suprasternale	Distance	Stā. Dev.	0.57	0.71	0.41	0.51	0.39
t t	> 1	Mean	0.10	0.12	0.14	0.07	0.13
Menton	Distance	Std. Dev.	0.33	0.31	0.33	0.23	0.26
	e Z	Mean	-4.09	-3.57	-2.76	-2.27	-2.26
	Distance	Std. Dev.	0.38	0.49	0.66	0.61	0.68

UPPER TORSO INFORMATION
Head Position 2

			SC I	II	III	IV	v
	ė	Mean	1.78	1.64	1.75	1.55	1.61
	Distance	Std. Dev.	0.91	0.72	0.47	0.42	0.42
Q	×	Mean	-0.94	-0.68	-0.09	0.19	0.24
Suprasternale	Distance	Std. Dev.	0.55	0.61	0.46	0.50	0.66
to	×	Mean	0.02	0.11	0.03	-0.01	0.03
Menton	Distance	Std. Dev.	0.23	0.20	0.16	0.21	0.35
	Z =:	Mean	-1.43	-1.35	-1.67	-1.45	-1.41
	Distance	Std. Dev.	0.86	0.71	0.49	0.43	0.45

UPPER TORSO INFORMATION Head Position 3

			SC I	II	III	IV	V
	e	Mean	7.09	6.815	5,82	5.373	5.42
	Distance	Std. Dev.	0.73	0.77	0.98	1.24	1.16
O)	×	Mean	-1.72	-0.56	-0.81	0.42	0.49
Suprasternale	Distance	Std. Dev.	0.69	0.78	0.68	0.88	0.90
t	¥	Mean	0.22	0.25	0.13	0.04	0.09
Menton	Distance	Std. Dev.	0.37	0.31	0.36	0.43	0.51
	ce Z	Mean	-6.83	-6.73	-5.71	-5.28	-5.32
	Distanc	Std. Dev.	0.78	0.81	1.02	1.17	1.10

UPPER TORSO INFORMATION Head Position 4

			SC I	II	III	IV	v	
	è	Mean	5.62	5.40	4.84	4.60	4.48	
	Distance	Std. Dev.	0.64	0.69	0.82	0.85	0.91	
ø	e X	Mean	0.38	1.12	1.69	2.13	2.11	
Suprasternale	Distance	Std. Dev.	1.03	0.99	0.68	0.73	0.77	
ᅌ	е У	Mean	4.21	4.13	3.90	3.64	3.53	
Menton	Distance	Std. Dev.	0.60	0.61	0.57	0.59	0.66	
	z ə	Mean	-3.55	-3.13	-2.19	-1.74	-1.59	
	Distance	Std. Dev.	0.45	0.48	0.71	0.49	0.71	

UPPER TORSO INFORMATION Head Position 5

							
			SĊ I	II	III	ΙV	٧
	a	Mean	4.29	4.49	3.91	4.08	3.92
	Distance	Std. Dev.	0.66	0.79	0.47	0.53	0.63
e	x ec	Mean	0.76	1.37	1.57	2.07	1.86
Suprasternale	Pistance	Std. Dev.	0.90	0.89	0.46	0.46	0.52
to	>	Mean	3:67	3.77	3.43	3.44	3.37
Menton	Distance	Std. Dev.	0.56	0.61	0.45	0.48	0.60
	e Z	Mean	-1.86	-1.75	-0.86	-0.51	-0.39
	Distance	Std. Dev.	0.61	0.67	0.46	0.44	0.39

UPPER TORSO INFORMATION Head Position 6

			SC I	II	III	ΙV	٧
	ه	Mean	6.95	6.52	5.87	5.62	5.43
	Distance	d. Dev.	0.77	0.78	0.88	1.05	0.97
		Std			······································		
a	×	Mean	0.42	1.31	1.51	2.57	2.58
Suprasternale	Distance	Std. Dev.	1.11	1.23	1.17	1.17	0.94
to	>	Mean	3.69	3.28	3.04	2,91	2.92
Menton	Distance	Std. Dev.	0.60	0.73	0.99	0.82	0.76
	ce Z	Mean	-5.72	-5.30	-4.56	-3.86	-3.61
	Distan	Std. Dev.	0.92	0.77	0.87	0.90	0.89

APPENDIX A-3
Hand-arm Rest Data

	0 O	*																																			•
	Z-STAND DEVIATIO	* * * * * * *	30	8	-	-	6	8	8	0.86	7.	3	-	1.	-7	9.	7.	- 7	Š	•6	•	S.	•6	8	8	4.	9.	ŝ	Š	4.	•	- 7		1	• 6	ŝ	i,
	Z-MEAN	***	2.3	7.6	3.0	4.9	1.9	1.9	2.4	30.66	5.9	2.3	3.0	0.2	0.3	o.8	5.9	1.2	8.6	7.8	ŝ	5	6.	2.1	7.7	4.	4.0	0	6	6.3	2.4	6.2	9.	4.1	7.	.2	•
	Y-STAND DEVIATION	***	9	5	4.	4.	0	3	2	0.52	3	4	'n	9	4.	~	ů	S	4	~	9	4.	4	-	9.	~	6	9.	4	7	0	•	S	1.	-	4.	
	Y-MEAN	***	6	4.	å	.7	8	10.2		0.20	4	4.	6.0	10.0	0.2	10.4	7.	•2	6	6.9	0	10.3	10.4	7	•2	•	9.9	10.0	4.0	10.5	7	•2	3	6.8	10.3	0.3	10.4
-4	X-STAND DEVIATION	****	0	0	•	0	4.	• 6	8	1.02	5.	9.	8	4.	9.	8		6.	.7	0	7.	6.	0	• 2	?	Φ,	6.	6.	7.	~	•	6.	8	φ.	6.	• 2	٠,
PCSIT	EA	***	7.	₹		0.3	3	3	0	60.0	4.0	6.	5.5	3	9.	7.	6.6	9.	9.8	3.7	4.	0	3	5.5	4.1	13.8	1.1	•5	7	8	16.3	6.4	3	18.3	•		4.
H	SAMPLE SIZE	*	23	23	23	24	54	24	24	54	24	24	24	24	24	54	24	54	24	54	24	54	24	54	24	54	77	54	5.4	54	77	54	77	77	54	54	54
	POINT NO.	**	-	7	m	4	5	9	7	-4	7	m	4	S	9	7	- -4	7	m	4	Ŋ	9	7	-4	7	m	4	ហ	9	2	~	7	m	4	3	9	7
	SEAT PAN ANGLE	****	01	07	10	10	01	01	70	70	70	10	01	10	01	07	10	10	10	01	01	10	10	10	10	01	10	01	10	07	20	20	70	20	20	50	70
	BACK REST ANGLE	****	13	13	13	13	13	1.3	13	27	27	27	2.2	27	27	2.7	51	51	51	51	51	51	51	65	65	65	99	92	65	65	65	65	99	65	9	65	65

	Z-STAN	~ * > *	5	6	~	~	ထ္	သ	8	0.85	8	ŝ	~	-	•	9	9	ທ	ŝ	9	•	ň	ŝ	-	~	4	'n	8	Š	4	~	~	4	~	~	ď	'n
	Z-MEAN	***	2.2	7.5	3.5	4.8	1.8	1.7	2.5	30.63	5.9	2.3	2.9	4.0	0.2	0.7	5.9	1.2	8.5	7.8	8.5	9.	6.	2.1	1.	5.4	4.2	•	7	6	2.3	6	5.6	4.3	7.5	3	Š
	Y-STAND	* * *	9	S	, T	*	~	6	7	0.52	3	4.	9	9	w	4	4	4	4	è	7.	W	3	•	'n	9.	8	9	ų	4	'n	1	9	1	9	4	2
	Y-MEAN	***	6	4	9	6.7	10.0	~	10.3	0.22	i,	4	6.9	9.6	10.2	4.0	0.2	7	4	•	9.7	10.1	0.3	7	7	4	8	1.6		10.4	.2	7	4	6.9	7.6	10.2	0.3
I ON 2		* * * * * * * * * * * * * * * * * * *	~	9	9	6.	4	-	3	1.17	9		6.	4.	9	8	7	6	7	6	6.	0	7	7	8	æ	8	ø	0	7	0	9	0	8	0	4	4
CSIT	X-MEAN	***	-	~	Ÿ	∹	ů	4.	5.0	60.0	4	1.8	•	4.	6.1	7	8.6	3	9.8	7	3.4	6.8	*	5.4	14.1	3.7	6.8	4.	Ç.	S	6.3	6	5. 5	17.4	1	Š	-
⋖	SAMPLE	4 ¥	54	54	24	54	24	24	54	54	77	54	54	54	54	54	24	24	77	54	54	24	54	23	23	73	23	23	22	23	23	23	23	23	23	23	23
	POINT	***	-4	7	M	4	2	9	_	~	7	m	4	J.	9	_	-4	7	m	4	Ŋ	9	7	~	~	m	4	Ŋ	9	7		7	M	4	S	9	_
	SEAT PAN	*******	01	10	10	01	91	07	01	07	01	01	10	10	9	01	10	01	01	01	70	01	10	01	07	01	01	01	70	01	20	70	20	20	20	20	20
	BACK REST	*****	13	13	13	13			13	27	27	2.7	27	27	27	27	15	15	51	21	51	51	51	65	65	· 62	62 '	65	92	92	65	65	99			69	

-	DEVIATION	* * * *	0.83	CL3	ய	_	Cr.	v	•	_		, ,	1 '			•	~ .		-		•		_		•	_	•	•		•								,	•
	Z-MEAN	* * * * *	32.32	9",	3.7		1.7	7.1	4		•	, ,	7	2	•	v	8	3.0	_	8		-:		•	2.	-	Š	_		•		•			•		•	•	•
i	Y-STAND	* * *	'n	•		4		. 4		יי	י י	75.0		9	-	94.0	4	4	~	4		_	•	• • •	7		٠.	0.84							•	•	•	•	•
	Y-MEAN	***	\sim	~		œ	10.0		- 6	7.07	~	v	ຜາ	ó. S	1.6	10.1	, 4	0				0			6			-6.85	0	3	101			•	•		•		•
8	X-STAND	- * : *		ď	4) α) ડ	Ρ,	0 (20	ຫ	Or.	Φ	Q,	7	w	···	•	, •	_			_			-		76.0				•	•	•	•		•	•	•
S	-MEAN	* * * * *	4) (֓֞֜֜֜֜֜֜֜֜֜֜֜֜֜֜֓֓֓֓֜֜֜֜֜֜֜֓֓֓֓֓֜֜֜֜֓֓֓֡֓֜֜֜֡֓֡֓֜֜֜֡֓֡֓֡֓֡֡֓֡	•	0 '	7.	5	\mathbf{c}	v	w		C	6	, (• •		0	, ,) (1	•		. CT	• •	-17 07	• • u	e n u	•	• •	• •				•	•	•
H	MPLE	*****	70	7,0	* 7 6	*7	47	54	54	24	24	24	70	26	26	26	26	7 7	77	7,0	77.	47	57	57	5 7	57	47	47	57	4 7	47	57	23	23	23	23	23	23	23
	POINT	** ** **	•	٠, (7 (.	4	S	9	7	-	I (\)	ות	1 4	ه ۲	n 4	9 1		٠,	7 (η,	† (N.	9	_	 4 (7	M ·	\$ (v .	9	1	~	7	m	4	S	, v c	~
	SEAT PAN	ANGLE ******	•	01	10	10	07	01	70	10	0	2 -	2 -	3 -	2 .	0.	0 .	01	01	67	01 :	07	70	01	07	01	01	01	01	10	10	01	70	20	20	20	20) (·	20
	ACK REST	ANGLE		13	13	13	13	13	13	۲-	1 6	17	17	7.7	17	27	27	27	15	51	51	21	51	51	51	65	65	65	65	65	65	65	65	65	65	, (C	, r	3 4	65

N X	_								_	_	_	_			_	_					_			_	_		-	_	_	_	_				
2-STAN DEVIATI *****	æ	6.	7.	-7	8	8	1.	0.85	ထ္	•6	7.	8		7.	1.	9.	'n	•6	7.	.5	3		8	4.	4.	5	5	ŝ	9	.7	4	3	4	•	S
Z-MEAN *****	2.3	7.6	3.5	4.8	1.9	1.8	2.4	30.59	5.9	2.3	2.8	1.2	0.2	9.0	5.9	1.2	8.5	1.9	6.6	6.	0.	2.3	7.9	5.	4.4	7.	5	4.	2.5	8.1	7.	4.5		8	~
Y-STAND DEVIATION ******	9	5	4	4	ø	4	3	0.54	S	'n	'n	~	3	3	4.	4	n	4	S	3	5	ó	ď	Ň	۲.	Š	4	5	5	ď	•	9	ù	4.	ď
Y-MEAN	ι,	3	9	1.	Ö	0.0	7	0.15	7.	4.	6	α	0.1	.2	5	0	'n	2	4.	0.0	2	7.	0	3	6	3	0.1	4	0	0	4	7.0	9.3	Ç	0.2
ION 4 X-STAND DEVIATION *******	7.	0	• 6	G	4.	7.	6	1.15	0	• 6	0	5	- 1	6.	2.	6.	1.	1.	8	0	.2	• 2	0	6.	8	8	6.	0	٦.	6	1.	8	6	7	
POSIT	9	7	.2	9	4.	.5	6.9	10.0	3	6	.2	3	•6	5.2	6.6	3	7.	4	1.4	9	4	5.5	4.0	3.5	•	3.5	7.	0.3	7	4.7	4.1	0	3.9	•2	8
HAND SAMPLE X- SIZE *****								54																											
**************************************		7	m	4	Ś	9	7	~	7	m	4	Ŋ	9	7	7	2	ო	4	ß	9	7	-4	7	m	4	ιν	9	7	1	7	m	4	Ŋ	9	~
SEAT PAN ANGLE		10	10	10	01	10	10	01	70	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	10	07	20	20	20	20	20	20	20
ACK & EST ANGLE ******	13	13	13	13	13	13	13	27	27	2.7	27	27	27	27	51	51	51	51	51	51	51	65	65	65	65	65	65	65	65	65	65	65	65	65	92

HAND PCSITION 5 SAMPLE X-MEAN X-STAND Y-MEAN Y-STAND Z-MEAN Z-STAND SIZE SIZE DEVIATION ARREST RRESHER	4 5.75 1.i6 0.33 0.64 32.31 0.8	4 5.14 1.07 0.44 0.55 27.58 0.8	4 3.28 0.70 0.63 0.49 23.49 0.7	4 0.24 1.05 -6.85 0.45 24.69 0.7	4 3.57 0.53 -9.66 0.80 11.71 0.9	4 13.45 0.77 -10.02 0.35 10.12 0.8	4 17.05 0.92 -10.28 0.34 10.52 0.8	94 0.17 0.56 30.47 0	4 -0.38 0.98 0.31 0.50 25.83 0.7	4 -1.86 0.60 0.48 0.46 22.30 0.6	4 -5.00 0.93 -7.08 0.47 22.82 0.7	4 1.69 0.45 -9.84 0.67 10.97 0.7	4 11.57 0.72 -10.08 0.51 8.65 0.7	4 15.25 0.90 -10.29 0.29 8.75 0.7	4 -9.91 1.30 0.16 0.38 25.94 0.6	4 -9.58 0.97 0.19 0.40 21.27 0.6	4 -9.74 0.76 0.38 0.32 18.53 0.5	4 -12.67 0.64 -7.19 0.46 17.98 0.5	4 -1.41 0.92 -9.47 0.52 10.49 0.8	4 8.83 1.08 -10.13 0.42 9.55 0.5	4 12.43 1.24 -10.30 0.37 9.91 0.5	4 -15.55 1.14 0.25 0.47 22.20 0.7	4 -14.15 1.00 0.20 0.44 17.79 0.8	4 -13.63 0.91 0.46 0.57 15.49 0.5	4 -15.91 0.82 -6.89 0.78 14.43 0.4	4 -3.55 0.87 -9.36 0.71 8.95 0.6	4 6.74 1.02 -10.08 0.41 8.07 0.6	4 10.36 1.12 -10.31 0.38 8.21 0.5	3 -16.18 1.10 0.05 0.52 22.51 0.7	3 -14.65 0.92 0.06 0.58 18.12 0.7	3 -14.18 0.80 0.38 0.61 15.73 0.3	3 -16.34 0.86 -6.99 0.68 14.60 0.6	3 -3.91 0.94 -9.30 0.67 9.28 0.5	
	.75	014 100	.28 0.7	.24 1.0	.57 0.5	3.45 0.7	7.05 0.9	•24 0.9	0.38 0.9	1.86 0.6	5.00 0.9	69. 0.4	.57 0.7	5.25 0.9	9.91 1.3	9.58 0.9	9.74 0.7	12.67 0.8	1.41 0.9	.83 1.0	2.43 1.2	15.55 1.1	14.15 1.0	13.63 0.9	15.91 0.8	3.55 0.8	.74 1.0	0.36 1.1	16.18 1.1	14.65	14.18 0.8	16.34 0.8	3.91 0.9	1.1
AMPL SIZE	7	N	7	7	7	7	7	1 24	2	2	2	2	2	2	2	2	7	54	7	2	2	54	54	57	24	2	2	2	23	23	23	23	2	•
SEAT PAN PO ANGLE N ******	10	01	01	10	10	01	10	10	01	01	01	01	70	01	01	70	01	70	10	10	10	01	01	01	01	01	10	10	20	70	20	70	20	000
ACK REST ANGLE	13	13	13	13	13	13	13	77	27	27	2.7	27	27	2.7	51	51	19	51	75	51	51	65	65	65	65	65	9	65	65	65	65	65	65	45

N *																																			
Z-STAND DEVIATIO ******	0.82	•	•	•				0.70	•	•			•	•	•	•	•	•	•		•		•		•							•			•
Z-MEAN *****	32.30	7.6	3.4	4.5	1.5	'n	9	0.5	5.9	2.2	9	0.8	7	8	5.8	1.1	S	7.9	1.1	1.3	1.9	2.2	۲.	5.4	4.4	1	. 7	0.1	2.4	8.0		4.5	6.6	0.0	4
Y-STAND 3EVIAT ION ******	0.61	ŝ	4.	4.	7.	.2	4	9	ď	4.	i,	S.	ú	4	6	4	4.	₹.	9	3	4	3	3	9	9	7	4	7	4.	4	ð	8	ø	ď	m
Y-MEAN	0.27	~	•	Φ,	-	6.6	7	7	7	4.	9	7	0.0	10.2	₹	7	u,	9	ď	7	10.2	7	7	4	8	N	၁	0.3	0	0	ú	0	4.6	0.1	-10.30
I GN 6 X-STAND DEVIATION ******	1.08	•	•	6	S	7.	3	6.	9		6.	'n	. 7	8	.2	9	œ	8	φ,	•	7.	.2	10.1	8	.7	8	6.	7	S	6.	7.	a	6.	7	.3
PCSIT-MEAN	5.84	.2	u	4		3.3	8	7	ن	-1.80	•	7	4.	5.0	8	•6	8.6	2.9	•2	8.9	'n	5.5	14.1	3.6	0.9	ď.	6	9.0	16.2	4.8	4.2	•	8	4.	0
HAND SAMPLE X. SIZE *****	54	24	54	54	54	54	54	54	54	54	54	54	54	54	54	23	54	24	54	24	24	24	54	24	54	23	23	23	23	23	23	23	23	23	23
FOINT **	-4	7	m	4	Ŋ	9	7	-	7	Ю	4	S	9	7		7	m	4	S	9	7	 4	7	ന	4	ß	9	_	~	7	æ	4	'n	9	7
SEAT PAN ANGLE	. 01	10	01	10	70	70	10	10	07	10	10	01	10	01	10	70	70	10	01	70	10	01	07	70	07	07	70	01	20	20	20	20	20	20	20
BACK REST ANGLE ******	13	ដូ:	13	13	13	13	13	27	27	27	27	27	27	27	51	51	51	51	51	51	51	99	92	99	65	65	65	65	65	65	65	65	99	65	65

ostinistinanun tekun soliteisisteken Kaskatán sepanjakh jestinán elektriketek pelektriketek jestek pelektrike

Elbow Joint Position for 5th to 95th Percentile as a Function of Seat Configuration for Hand Position 1

Coordinates	p=4	11	III	١٨	^	Percentile
×	50	-1.85 -2.59 -3.33	-4.22 -5.44 -6.66	-5.80 -7.27 -8.74	-6.15 -7.68 -9.21	95th 50th 5th
Z	13.50 11.98 10.46	11.55 10.28 9.01	8.54 7.50 6.46	6.93 6.01 5.09	7.15 6.14 5.13	95th 50ch 5th
Displacement X		-2.13 -2.09 -2.05	-4.50 -4.94 -5.38	-6.08 -6.77 -7.46	-6.43 -7.18 -7.93	95th 50th 5th
Z		9. 4.	6.4.0	ນີ້ວ		95th 50th 5th

APPENDIX A-4
Hand-arm Rest Data

DEST AVAILABLE CON

BR=65SP=20 LENGIF ALPHA BETA	1 170.4 5 165.8 7 168.0	10.45 164.3 140.5 10.63 168.9 138.9 10.55 164.3 144.1 10.28 166.0 146.5	165.9	10.75 166.1 144.3 11.22 163.3 147.5 10.09 164.0 140.9 10.75 161.2 143.1 9.83 163.1 142.4	165.6 165.8 163.8 164.6 164.5 166.2 165.9	10.80 165.0 143.1 0.54 2.0 2.6
ELBOW ORIENTATION BR=b5P=10 LENGTH ALPHA BETA	170.8 16.771 16.771	10.44 166.4 140.4 10.06 160.6 141.0 10.51 103.7 142.5 10.76 157.8 150.1	164.6	10.95 163.8 142.3 11.50 165.0 140.4 20.10 161.9 142.1 10.70 165.0 140.1 10.25 161.0 139.4	164.1 164.1 164.2 164.8 164.8 164.8	10.89 164.3 142.4 0.42 2.6 2.7
ELBGW 10 STYLION ANGLE IATEC WITH ACROMIALE-ELBOW BR=51SP=10 LENGTH ALPHA BETA LEN	168.9	10.42 166.8 124.5 10.34 167.6 124.9 10.69 161.0 128.5 11.39 163.2 136.0	164.6	11.37 162.9 128.4 11.24 165.4 132.5 10.13 165.1 124.4 10.73 164.7 127.2	10000000000000000000000000000000000000	10.86 165.2 128.6 0.49 2.0 3.0
HAND PUSITION I LENGTH IS DISTANCE FROM ELB ALPHA IS ITS ASSOCIATED ANG BETA IS THE ANGLE ASSOCIATE BR=275P=10 LENGTH ALPHA BETA LE	166.8	10.38 164.5 98.6 10.50 167.7 98.5 10.41 160.3 103.6 10.33 166.0 111.4	163.6	10.54 167.7 101.8 10.55 165.4 108.6 10.50 164.4 97.4 10.88 163.5 105.2	165.0 167.0 167.0 163.0 163.1 163.8 163.8	10-60 164-9 103-0 0-38 1-9 3-9
H L B B B LENGTH ALPHA BETA	166.4	-	167-6		164.7 162.0 162.0 164.0 161.8 161.8	10.50 163.8 89.3 0.47 2.1 4.6
SUBJECT	- N N N	4001	860	12211	116 118 22 23 24 25 25	MEAN VL STD DEV

BR=65SP=20 LENGTH ALPHA BETA	11.12 164.9 151.0 11.90 160.0 149.4 12.04 159.9 151.1 10.57 161.4 145.0		155.6 155.6 157.0 154.3 159.8	152.6 159.9 159.9 152.6 157.0	10.69 162.8 149.5 10.46 158.4 148.0 10.85 160.7 151.8 11.11 158.7 149.8 0.50 3.3 3.1
LBOW ORIENTATION BR=65SP=10 LENGTH ALPHA BETA	166.9 164.6 158.9	10.56 162.0 145.3 10.56 162.0 145.3 10.30 152.7 154.4 11.76 158.9 151.9 11.35 157.0 147.3	158.8 156.4 156.8 159.2	10.97 154.0 150.6 11.51 155.4 152.1 11.52 170.2 139.9 10.76 153.3 150.0 11.78 156.1 149.1 10.90 157.4 145.2	
ELBOW TO STYLION ANGLE (ATED MITH ACROMIALE-E) BR=51SP=10 LENGTH ALPHA BETA ************************************	11.19 161.5 135.9 11.57 157.1 138.2 12.24 158.9 140.8 10.30 166.8 126.5	165.0 157.3 157.6 164.1	159.7 162.4 157.1 160.1		162.3 158.5 157.4 159.7 3.3
AND PCSITION 2 ENGTH IS DISTANCE FROM ELBOW TO STYLION LPMA IS ITS ASSOCIATED ANGLE ETA IS THE ANGLE ASSOCIATED WITH ACROMIALE-ELBOW ORIENTATION BR=27SP=10 LENGTH ALPHA BETA LENGTH ALPHA BETA LENGTH ALPHA I REGENTATION REGENTATION	10.72 166.2 117.5 10.90 165.3 114.4 11.59 165.2 113.4	161.3 156.6 164.3 162.6	161.7 163.1 165.4 162.2 160.3	162.6 161.0 165.6 160.9 163.6 165.1	10.29 163.6 113.3 9.94 163.6 108.2 10.55 165.2 111.4 10.63 163.0 111.8
HA LE BR=13SP=10 LENGTH ALPHA BETA	11.32 168.0 95.8 11.14 164.7 98.4 11.09 164.9 96.9	169.4 169.4 169.4 169.4 160.1	164.4 166.1 162.8 162.4 163.6	164.6 164.6 164.6 164.2 165.2 163.1	10.06 159.4 104.8 9.35 162.1 88.7 10.41 166.0 95.3 10.39 163.8 97.4 0.53 2.5 4.4
SUBJECT	- N M 4	* ~ ~ ~ ~ ~	0 1 2 6 4	12 13 14 16 17 18 17	22 2.3 2.4 2.4 MEAN VL STD DEV

BEST AVAILABLE COPY

			+	*	6.	6.	6	6	9•	0	.3	٥.	9	•		6	4.	-2	8	8.	9•	89		•	.2	4.	6.	6	4	•	2
		0=20	A 8ET	* * * *					4 148.6				8 153.6					0 151-2				1 151				9 150.4			7 152	•	n 2
		BR=65SP=20	ALPHI	*	166.6	167.7	162.7	165.8	168.4	168.4	161.8	167.9	163.8	161.2	160.5	164.7	162.9	165.0	159.9	168.1	166.5	159.		164.1	164.0	169.9	164.3	165.	164.		1
		BR	LENGTH ALPHA	计算 计分类系统 计分类	11.03	11.17	11.80	10.25	10.84	10.23	10.45	10.94	10.90	11.89	10.98	11.25	10.22	10.42	10.15	10.54	10.99	10.72		11.46	10.00	10.30	10.45	10.65	40.77 164.7 152.4		10.0
	z	10	3E TA	****	6.651	143.5	153.0	147.0	151.9	148.3	160.5	153.8	149.6	148.8	149.4	155.3	151.9	152.9	151.5	150.8	141.5	153.2	149.4	154.0	148.7	149.0	149.9	149.9	0.151	0.17, 7.701	•
	ITATIO	dk=655P=10	LPHA		171.4	4.691	165.6	9.021	166.0	168.5	158.2	165.6	165.6	160.4	166.3				160.5		177.3	158.3	163.9	159.4	162.1	169.0	166.5	168.6	45.5		4.0
	hITH ACROMIALE-ELBOW ORIENTATION	140	LENGIH ALPHA	化苯甲基苯甲基甲基苯甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基甲基				-			-											10.79						10.51	107.01	7	***0
8	MIALE-EI	10	BETA	****	137.1	135.4	140.0	127.8	131.6	138.3	141.1	139.4	137.4	139.0	133.7	143.7	133.5	141.4	142.1	141.4	136.6	144.4	137.9	143.6	136.4	136.6	141.4	141.1	7 021	1-967 0-997	7.4
TO STYLION	ACRO	BR=515P=10	LPHA	****	172.2	168.3	170.4	174.1	173.8	162.0	162.3	174.1	161.3	164.5,	170.1	163.0	6.80	161.5	161.2	4.591	171.2	161.4	167.3	160.7	166.4	171.6	162.1	165.5	7 77	00	4
	ANGLE Ated Mith	BR=	LENG TH ALPHA	安武 安安 安安 等 医骨头 医 电电子 的	10.59											•						10-62								70.01	7<0
CE FROM	HA IS ITS ASSOCIATED ANGLE A 1S THE ANGLE ASSOCIATED	10	BETA	****	119.2	112.3	113.5	104.2	111.6	113.9	115.3	112.7	116.6	111.2	116.8	112.6	106.8	112.2	109.9	113.9	107.8	117.7	109.5	103.6	106.0	111.2	106.9	111.6		1111	* * *
ISTAN	SASS	BR=275P=10	LPHA	****	151.6	166.2	6.85T	150.9	152.4	153.0	5c.8	1.451	54.7	54.1	51.0	55.3	53.1	52.0	53.9	52.7	56.7	152.4	156.0	56.3	155.8	58.0	156.3	157.1		7.001	3.2
ENGTH IS D	ALPHA IS ITS ASSOCIATED ANGLE RETA IS THE ANGLE ASSOCIATED	38.	LENSTH ALPHA	安然的女 化安全等非常存在 化安夫拉夫	11.68				11.06	10.66	10.88	11.30	10.96	11.51	11.45	11.31	11.02	10.85	10.22	11.35	11.62	10.79	11.58	11.40	10.16	10.73	10.46	10.98		7.661 10.11	0.4V
3	¥ 6		Ē	*	1-66	100.3		92.7		4.46	106.7	90.7	101.9	96.8	93.9		95.2					102.9		89.5	7.46	100.9	666	95.8		9.76	3.7
		=13SP=10	LPHA	* * * *	61.3	2.5	9.2	0.	53.6	6.5	.3	56.3	53.1	55.5	58.4	53.0	51.1	53.6	54.3	56.3	56.2	154.7	54.9	57.	57.	55.0	64	58.5		155.5	2.8
		BR=	ENGTH		11.71 1	11.61	11.40	10.63 15	10.73	10.27	10.60		10.87									10.46 1				19.75 1		10.74 1	•	_	
			SUBJECT		-							80	• •	10	11	12	e	14	· ~	1 -	1	18	16	20	212	22	1 (57	; • ;	MEAN VL	STD DEV

155.2 155.2 155.2 155.2 155.2 155.2 155.2 150.5 150.5 150.5 150.5 150.5 150.5 150.5 150.5 150.5

		HAND POSITION 4 LENGTH IS DISTANCE FROM	ELBGY TO STYLION		
		ALPHA IS ITS ASSOCIATED BETA IS THE ANGLE ASSOCI	ANGLE ATED WITH	LBOW ORIENTATION	
	BR=135P=10	BR=27SP=10	<u>;</u>	BR=65SP=	ï
SUBJECT	LENGTH ALPHA BETA	LENGTH ALPHA BETA	LENGTH ALPHA BETA	LENSTH ALPHA BETA	LENGTH ALPHA BETA
	*	* * * *	餐茶 新价格 经销售货票据 经销售证券 新种	医法律检查 医安全性病 化聚苯酚苯甲基	女孩 化水油 医水油 医水油 医水油 医水油 医水油 医水油 医水油 医水油 医水油 医
_	11,17 165,7 107,8	11.73 151.5 125.0	10.90 lol.6 138.9	10.93 164.2 152.5	163.4
• 0	84 142-9 105-	158.9 125.	155.3	158.	156.2
4 "	46 161.3		12.79 152.2 150.7		12.20 155.6 155.0
1 4	10 163.2	164.0	164.5	158.0	153.8
٠.٠	7 162.1	155.5	160.1		
• •	9.58 166.7 103.6	158.2 1		156.7	156.3
7	.86 167.8	155.0		155.9	156.1
දා	.85 164.5	160.2	155.5	155.8	153.9
6	163.6			11.45 153.7 152.6	153,1
10	164.2	158.3	148.9	150.9	152.8
11	164.6 1	157.1	11.52 151.9 143.8	154.1	150.7
12	163.2 1	156.4	150.6	154.1	154.3
13	162,3 1	154.2	154.7	154.1	
14		157.7	154.5		159.9
15	163.8 1	160.2	150.7	150.9	153.4
16	_	158.7	152.5	8 153.7	155.6
17	165.2	158.4	156.2	165.2	158.0
81	161.2 1	161.0			155.8
19	7	161.8	156.8		
20		6.091	~	156.5	156.5 152
21	156.0 101.	10.18 162.7 111.6	10.34 154.0 141.8	152.6	156.0 153
2.2	3.1	10.43 159.8 124.3	2.0 141.	7 158.8 152.	162.8
23		163.1 L	48 152.5 14		10-42 156.8 152.6
24	10.28 164.1 102.3	164-1 115-	5.1 145.	B 159.4 154.	158.6
NA MA	10.47 163.7 104.8	10.79 159.1 120.4	11.21 154.8 143.6	11.22 156.2 152.7	11.20 156.1 153.2
STD DEV	1.8	3.1	4.0	3.6	3.1

BEST AVAILABLE COPY

DIST AVAILABLE CON

BR=65SP=20 LENGTH ALPHA BETA	170.5 163.2 164.9 162.4			170-1 163-5 162-2 162-7 176-1 164-1	0.54 3.5 3.0
LBOW OXIENTATION BR=65SP=10 LENSTH ALPHA BETA	172.1 166.4 164.6 166.6		160.0 157.2 163.7 165.4 159.5		10.76 164.7 159.6 0.54 4.3 2.9
ELBCM TO STYLION ANGLE ANGLE ANGLE BRE51SP=10 LENGTH ALPHA BETA ************************************	175.4 144. 159.9 152. 160.1 157. 177.9 137.	175.6 164.2 164.2 171.1		168.0 160.2 109.5 164.0 164.0 169.4 161.3	10.56 165.6 149.7 0.62 5.8 4.7
AND POSITION 6 ENGTH IS DISTANCE FROM ELBCNLPHA IS ITS ASSOCIATED ANGLE ASSOCIATED BR=27SP=10 LENGTH ALPHA BETA LENG	148.4 146.8 144.4 148.6	149.4 149.7 149.2 149.2		1144.5 144.5 144.6 144.6 144.6 144.6 144.6 144.6 144.6 146.6	11.40 145.0 119.7
HA LE AL BR=135P=10 LENGTH ALPMA BETA	150.7 1 140.9 1 150.8 1	~~~~	147.9 145.6 145.6 145.6 146.6	15000000000000000000000000000000000000	11.29 148.5 104.4
SUBJECT	~ N M 4	0 c - 0 c	6 5 4 3 3 5 F 0 .	118 118 222 233 243 243	MEAN VL STD CEV

APPENDIX A-5
Foot Rest Data

													-		-			STAN STAN	Banker .	A CONTRACTOR	1	-	Socration and a	į		1		V	•									15	55		
S-2	DEVIA: 10N	8	ဆို	•	7.	5	•	4.	8	0.79	-	ŝ	.7	• 54	• 59	44.	66.	+9•	.57	.57	• 70	.51	. 52	.37	989	3 69 •	, 92 •	. 44.	14.	יי		٠,	•	۱۹	~	ų,	Š	-	4.	œ ا	-
Z-MEAN	* * * * *	2.0	4	3.4	4.7	5.2	0.9	2.4	4.1	30.69	0.0	2.3	2.9	4.8	5.9	2.2	7 · · I	5.9	1.2	8.6	6.	4.2	5.7	1.9	4.3	2.1	• 6	5.3	3.8	9.0	~	7.7	.	2.3	8.	5.6	4.0	4.3	6.2	9.	4.3
Y-STAN	JE VIA-1JN	9	9.	5	9.	•2	4.	ŝ	30	0.52	S	3	'n	6.	3	4.	6	1.	'n	٦,	9	~	4.	•	~	•	•	•	- 1	0	η,	٠, ١	•	Ĵ.	4	S	7.	Š	4	~ 1	~
Y-MEAN	**	ß	7.	1.	6.5	7.1	5.0	9.	4.9	0.30	4.	4.	6•9	7.1	7	7.7	6.5	7	۳,	3	0	7.3	n	1.9	9.9	•2	ب	س	1	7.5	5.4	-	6. 6	•	7	·5	6.7	4	5.3	7.6	.
N 1 X-STAND	→ * > *	0	0	. 7	• 2	0	0	6	3	96*0	0	9.	6.	•	8	-	4	• 2	6	φ.	3	. 7	٠,	• 9	• 2	7	• 9	6	0	ထ	φ,	~ `	7.	. 2	6		0	8	-		'n
OOT PGSIT	***	9.	6	₹	•2	9.	8.4		6.0	0.08	0.3	6.	4.	۲.	7.4	8.7	0.0	0.0	. 7	0.0	13.8	2.1	6.2	4.7	9.0	15.1	14.2	13.9	7.5	2.3	9	6.0	797	9	12.0	14.7	8.4	1.3	4.4	Φ,	0.
AP C.	######################################									24																															
POINT	** ** * *	~	7	ю	4	89	σ	70		7	2	ന	4	80		07		٦	7	M	4	80		01		-4	7	m	4	©		01		7	7	m ·	4	∞		01	
SEAT PAN	ANCLU ######	01	70	10	01	07	07	10	10	10	10	07	01	01	70	07	07	10	70	10	07	07	10	70	0.7	01	0	07	01	10	07	01	22	07	20	20	20	50	20	20	20
BACK REST	ANCI E # * * * * * * *	13	13	13	13	13	13	13	13	2.7	27	27	27	27	27	27	27	51	51	51	15	15	21	51	51	65	65	65	65	65	65	65	ر د ر	65	65	65	65	65	65	65	65

N Z-STAND DEVIATION ********	ر د		49.0	4 0 0	9.0	9°0	0 1 0	0 2.0	2 0.7	4 0.7	2 0.5	в 0.7	9.0	6 0 5	3 1.3	6 2.0	9.0	9.0	5 0.5	5 0.1	3 0.5	7. 0	1.4	3 1.5	9.0	6 0.7	8 0.3	†•0 •	1.1	9.0	1.5	9 1 9	9.0 6	2 0.7	4.0	9.0	5 0.7	3 0.4	
Z-MEAN	~	7	23.4	4.0	5.1	5	יניי	3.0	0.7	6.0	2.3	2.8	4.6	4.0	1.1	2.8	6.0	1.2	8.6	7.9	4.1	0	0.1	3.3	2.0	7.5	5.3	3.8	4.1	4.7	7	2.9	2.2	7.8	5.6	4.0	4.4	9	2.0
Y-STAND DEVIATION *******	ج.	, י	64.0	3	0	7	•	6	~	9	9	9	٥,	•	4	٦,	9	3	4	9	6	ω,	Š	7	9	9	۲.	7	Ö	Š	'n	30	4	4	Š	3	W	4	1
Y-MEAN ***	'5	, (0.68	6.8	7.6	0	7.6	6.5)	ŝ	ŝ	6.9	1.2	7	7.7	6.5	7	7	6	7.0	7.3	5.5	8.0	6.7	Ç	6	7	6.9	7.	5.6	8	0	7	.2	3	9.	.2	5.2	ď
1 ON 2 X-STAND DEVIATION	-	, 0	0.75	.2	0	0	4	.5	0.	6.	•	6.	•	8	7	S	.2	6.	. 7	6.	•	9.	0	7.	0	6.	6.	.2	-	~	~	~	7	6.	8	0	•	9	
OT PCSIT X-MEAN *****	ď	2	3.18	3	5	8.9	7	1.4	0	.2	1.8	3	3.6	8.2	9.5	. 7	0.0	9.1	0	3.8	8	6.9	6.7	9	15.5	14.1	3.9	17.4	2.3	6.3	4	6.8	6.2	15.0	14.7	8.4	3	7	4
FDI SAMPLE SIZE *****	24	24	57	24	54	54	54	24	54	54	54	24	24	24	77	54	54	54	24	23	24	24	24	54	54	24	54	24	24	54	24	54	23	23	23	23	23	23	23
*****	-	2	m	÷	80	σ	10	11	~	7	m	4	ထ	6	01	11	d	7	ю	4	80	6	10	11	7	7	M	4	co '	6	07	7 7	-	7	٣	4	80	6	9
SEAT PAN ANGLE	10	07	70	10	01	01	70	01	01	10	01	01	07	10	01	2	0	01	07	07	07	10	70	10	07	07	07	01	07	01	01	01	70	20	20	20	20	20	20
ACK REST ANGLE *****	13	13	13	13	13	13	13	13	2.7	27	27	27	27	27	27	27	15	21	51	15	25	51	15	75	9	65	. 65	ر ب	65	٥ ·	92	65	65	65	65	99	65	65	65

BEST AVAILABLE CONY

;	; ; ;	1	6	TISOG TO	8	1	ţ		
ACK KES! ANGLE	SEAL PAN ANGLE		SIZE	A-F	DEVIATION	Y-MEAN	V-SIAND DEVIATION	Z-MEAN	DEVIATION
****	***	***	*	***	* * *	***	* * *	* * * * *	***
13	07	-		. 7	.2	4.	. 7	2.1	8
13	10	2		7		3	9	7.4	8
13	01	m		7.	1	•	3	.3	•6
13	01	4		0	.2	8	ŝ	4.6	.7
13	07	80		e.	0	1.	6.	5.0	ŝ
13	10	σ		2.5	0	0	4	4.0	ထ္
13	10	01		9.	S	•	•	0.3	.2
13	07	11	24	6.1	9	9	.8	8	8
27	10	-		0	0	4	7.	9.0	٠,
2.7	10	7		0.3	6.	3	•	5.9	7.
27	10	ĸ		æ	9.	5	5	2.2	3
2.7	10	4		5.3	7	6.	4.	2.8	7.
2.7	70	90	54	٠,	7.	9.	.	4.5	3
2.7	10	6	24	8.8	8	?	4.	3.9	4.
27	10	10	24	1.6	7	6.	6.	0.2	
27	07	11	24	7.	5	ò	1.	8	6•
15	07	-4	24	0.0	7	7.	•	5.8	•
51	70	7	24	9.8	6.	•2	•	1.1	•
51	10	٣	24	0	8	.2	5	8.6	4.
51	10	4	23	3.7	8	7	'n	7.9	. 7
51	10	80	54	2.8	1.	4.	0	4.0	Ŝ
15	10	6	24	7.8	~	•2	• 2	3.9	4.
15	01	01	24	8.5	.2	ဆ	4.	0.1	•
21	10	11	24	ď	.2	5	.7	٦.	4.
65	10	-	24	15.5	٦.	7	•	2.1	•
65	01	7	24	4.1	6.	4	1.	7.6	۲.
65	07	m	24	13.8	8	3		5.3	ب
9	10	4	54	17.3	6	7.	~	3.8	4.
65	10	80	24	2.3	-	ŝ	6	3.9	•
65	70	o	54	7.0	8	S	4	4.0	'n
65	10	01	54	æ	W.	8	9	7.	4.
92	10	11	54	5.4	4.	0	. 7	7.0	•
99	20	-4	23	16.2		7	3	2.3	
65	20	7	23	6.4	6	.2	4.	7.8	
65	20	C)	23	. 7	-	7	Š	5.6	Ų
65	20	4	23	18.4	æ	ထ	9	4.0	9
65	50	œ	23	1.3	•	٥٠	7	4.1	~
65	20	Φ,	23	15.80	9.64	S	1.93	14.93	0.45
65	20	01	23	~	3	-	Ŋ	1.1	4.
65	20		23	8.0	4		α	2.6	.7

Function of	Percentile	95th	50th	5th	95th	50th	5th		95th	50th	5th	95th	50th	5th
as a	>	15.69	14.49	13.29	17.07	16.26	14.45		-4.40	-3.95	-3.50	03	25	. 53
th Percentile as Foot Position l	ΛΙ	16.99	15.65	14.32	17.02	15.73	14.44		-3.10	-2.79	-2.47	08	28	48
95t for	III	17.53	16.28	15.03	16.65	15.79	14.93		-2.56	-2.16	-1.76	45	22	.01
ion for Configur	II	18.88	17.44	16.00	16.86	15.90	14.94		-1.21	-1.00	79	24	-	. 02
of Knee Posit Seat	H	20.09	18.44	16.79	17.10	16.01	14.92							
о дот	Coordinates		×			7		Displacement		×			7	